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# **Argonne National Laboratory**

**TRANTEMP: A Code for Calculating  
Transient Temperature Distributions  
in Reactor Hydraulic Rabbit Facilities**

**by**

**Bryant N. Kristianson**

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Reactor Engineering Division

November 1968



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## NOMENCLATURE

<u>Symbol</u>	<u>Description</u>	<u>Symbol</u>	<u>Description</u>
c	Specific heat, Btu/(lb)(°F)	R	Radius (see Fig. 1)
$c_m$	Metal specific heat, Btu/(lb)(°F)	T	Temperature, °F
$c_p$	Specific heat at constant pressure, Btu/(lb)(°F)	$T_{bw}$	Bulk water temperature, °F
$c_w$	Water specific heat at constant pressure, Btu/(lb)(°F)	$T_w$	Wall temperature, °F
		$T_{1,2,3,\dots,8}$	Temperatures at radial nodes, °F
h	Heat-transfer coefficient, Btu/(hr)(ft <sup>2</sup> )(°F)	$T^{\circledR}$	Temperature at beginning of time interval, °F
$h_{1,2,3,\dots,8}$	Heat-transfer coefficients at radial nodes, Btu/(hr)(ft <sup>2</sup> )(°F)	$T^{\circledR}$	Temperature during time interval, °F
k	Conductivity, Btu/(hr)(ft)(°F)	$T^{\circledR}$	Temperature at end of time interval, °F
$k_m$	Metal conductivity, Btu/(hr)(ft)(°F)	V	Volume, ft <sup>3</sup>
q	Heating rate, Btu/hr	$\Delta r_1$	$r_2 - r_1$ , ft
r	Radius, ft	$\Delta r_2$	$r_3 - r_2$ , ft
$r_{1,2,3,\dots,8}$	Radii of nodes, ft	$\Delta r_5$	$r_6 - r_5$ , ft
t	Time, hr	$\Delta r_6$	$r_7 - r_6$ , ft
A	Heat-transfer area, ft <sup>2</sup>	$\Delta t$	Time interval, hr
D	Diameter (see Fig. 1)	$\Delta T$	Temperature increment, °F
$D_h$	Hydraulic diameter, ft	$\mu$	Water viscosity, lb/(hr)(ft)
G	Mass velocity, lb/(hr)(ft <sup>2</sup> )	$\rho$	Density, lb/ft <sup>3</sup>
Q	Volumetric heating rate, Btu/(hr)(ft <sup>3</sup> )	$\rho_m$	Density at metal node, lb/ft <sup>3</sup>
$Q_m$	Metal volumetric heating rate, Btu/(hr)(ft <sup>3</sup> )	$\rho_w$	Density at water node, lb/ft <sup>3</sup>
$Q_w$	Water volumetric heating rate, Btu/(hr)(ft <sup>3</sup> )		



TRANTEMP: A Code for Calculating  
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ABSTRACT

Written in FORTRAN for the CDC-3600 computer, the TRANTEMP Code (ANL designation: RE-418X) solves a set of numerical heat-balance equations. These equations describe the space- and time-dependent temperatures prevailing in a cylindrical, hydraulic rabbit assembly, which is heated by nuclear radiation and cooled by flowing water. Included are the mathematical model, the computer input specifications, a sample problem, and a FORTRAN listing of the code.

I. INTRODUCTION

Increased interest in advanced nuclear power plants has reflected a corresponding increase in the need for reactor test facilities for both short- and long-term irradiation of potential fuels and structural materials in environments approximating the high neutron fluxes, temperatures, and pressures anticipated in these plants.

Of the many types of static or dynamic irradiation facilities provided in research reactors and some production reactors, a most versatile type is the rabbit facility. Depending on the type of reactor and the experimental restrictions, small samples (rabbits) of candidate materials can be cycled into and out of the reactor core through pneumatic or hydraulic systems which penetrate the core. In either system, valuable irradiation data can be obtained up to the temperature, heat transfer, and hydraulic limits imposed by the reactor. The advantage of these systems is that, unlike some other types of irradiation facilities which require reactor shutdown for insertion of experiments, a large number of irradiations can be performed independently of reactor operation.

Coordination between reactor operation and safety is a vital factor in the planning, design, and hazards analysis of in-pile rabbit systems. Many of the experiment controls must be interlocked with reactor safety circuits to safeguard the reactor and experiment from potentially hazardous

conditions. System parameters or operating characteristics likely to promote these conditions must be interlocked with reactor control circuits to initiate reactor shutdown or to effect power reductions at a rate consistent with the nature of the hazard.

The array of vertical irradiation test facilities proposed for installation in the Internal Thermal Column (ITC) of the water-cooled and -moderated Argonne Advanced Research Reactor (AARR)<sup>1\*</sup> included five hydraulic rabbit tubes. These were to operate safely at all times; they were not to cause, contribute to, or intensify any potentially dangerous reactor conditions. Such conditions could have included creation of voids in the ITC, reactor power excursions caused by positive reactivity inputs associated with rabbit movement, and melting of the rabbit.

Some of these conditions could be attributed to certain heat-transfer problems which might be encountered during operation of the rabbit facilities. Of particular interest were problems of transient heating and heat transfer associated with reactor power fluctuations, changes in coolant flowrate, coolant flow reversal which prefaces rabbit removal operations, and rabbit movement. For example, the time elapsed during flow reversal will reflect a temperature rise in the rabbit and coolant and a fluctuation in the coolant pressure. An increase in coolant temperature, combined with a decrease in coolant pressure, could lead to boiling at the rabbit surface, with a possible resultant increase in reactivity due to void formation in the ITC, and a possible decrease in heat transfer from the rabbit. In such an event, a continued increase in the temperature of the rabbit could result in its partial or total meltdown. Under these conditions, a large surge of pressure resulting from flow reversal could terminate in failure of the rabbit facility tubing, if a proper reactor power reduction or total shutdown had not been effected. Thus, a method for computing the transient heat generation and temperature distributions was essential to a comprehensive design and safety analysis of the proposed installation.

Transient heat-transfer analysis in this case involves complex numerical calculations that are best performed with a digital computer. Because of deficiencies in available transient heat-transfer computer codes, a code was developed for analyzing heat transfer in the AARR hydraulic rabbit system under all transient conditions, including flow reversal and rabbit ejection. Appropriately entitled TRANTEMP and written in FORTRAN for a CDC-3600 computer, the code solves a set of numerical heat-balance equations which describe the space- and time-dependent temperatures in a cylindrical hydraulic rabbit assembly heated by nuclear radiation and cooled by flowing water.

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\*The AEC terminated the AARR Project in April 1968.

Although developed specifically for analysis of the AARR hydraulic rabbit system, the TRANTEMP code possibly can be used to analyze similar systems in other water-cooled reactors. To facilitate such use, this report describes the pertinent system and transient heat balance equations, gives the computer input specifications, details a sample problem, and includes a FORTRAN listing of the code.

## II. INTERNAL THERMAL COLUMN IRRADIATION FACILITY

Located centrally in the reactor core, the ITC contains an assembly (designated the ITC Facility) of nine vertical tubes for short- and long-term irradiation of encapsulated samples in a region of high thermal neutron flux (maximum unperturbed flux =  $5.5 \times 10^{15} n/(cm^2)(sec)$  at 100 MW). With reference to the plan view (Fig. 1), the assembly comprises five hydraulic rabbit tubes, two pneumatic rabbit U-tubes, and two static basket tubes. Long-term irradiations (several core cycles) are performed in the static basket tubes, which are inaccessible during reactor operation. Irradiations of a few milliseconds duration are performed in the fast-gas rabbit U-tube. Short to long irradiations (seconds to core life) are performed in the gas-cooled rabbit U-tube and the hydraulic rabbit tubes.

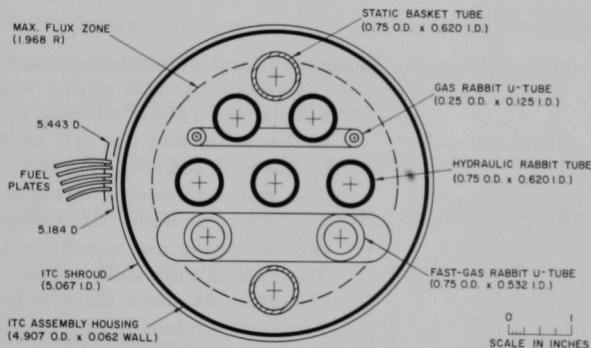


Fig. 1. Plan View of ITC Irradiation Test Facilities in AARR

The ITC Facility is a two-piece, interlocked assembly which penetrates a quick-opening closure plug in the reactor vessel. The lower, tubular section, which contains all the irradiation facilities, extends downward about 13 ft from the top of the reactor vessel and terminates just below the core. It is supported vertically by the quick-opening closure plug and laterally by guides above and below the core. During reactor fueling operations, the lower section is installed and removed as a one-piece unit. The upper section contains the fittings that interconnect with the various hydraulic and gas rabbit tubes; it is mounted atop, and breech-locked to, the closure plug. Sealing is effected by synthetic rubber O-rings.

During reactor operation, primary coolant flow is maintained through and around the lower section, the static basket tubes, and the hydraulic rabbit tubes by using the reactor-core pressure drop. Cooling water above the core enters each tube, flows down and around the sample, and discharges below the core. The outer surface of the ITC assembly housing is cooled by primary coolant, which flows through the annulus formed by the housing and the ITC shroud (see Fig. 1). Bulk ITC water within the housing is used to cool the outer surfaces of the irradiation-facility tubes; its velocity is kept intentionally low to prevent rapid introduction of voids in this area. Coolant enters the bulk ITC volume through ports in the ITC shroud, flows upward to the top of the lower ITC assembly housing and down through the housing, and discharges through holes in the rabbit tube lateral-support grid plate. A pressure differential of ~110 psi is available over the ITC facility.

The gas rabbit U-tube and the fast-gas rabbit U-tube are internally cooled by helium flow only when a sample is being irradiated. Heat generated by the in-core facility hardware is removed by the primary coolant water.

### III. ANALYTICAL DEVELOPMENT

#### A. Heat-transfer Model

The model used in the analysis is cylindrical in geometry. As shown in Fig. 2, it consists of the ITC-heated length of one hydraulic rabbit, the rabbit cooling water, the rabbit tube, and the ITC cooling water in the cell surrounding the rabbit tube. The water in each cooling system flows vertically at some time-dependent rate, the two rates not necessarily the same. The rabbit may also move in a vertical direction at some time-dependent rate. Time-dependent heat generation occurs throughout the heated zone. This heat is supplied by the reactor via gamma and neutron radiation.

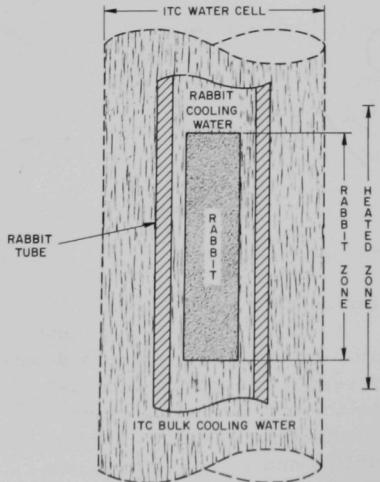


Fig. 2. Partial-section Schematic Diagram of One Hydraulic Rabbit Assembly

#### B. Assumptions, Conditions, and Basic Equations

The following assumptions, conditions, and basic equations are prerequisite to a numerical solution for a heat-transfer problem of this type:

1. All water present is assumed to be in the liquid state.

2. The "normal" water flow direction is downward.
3. The rabbit is a cylinder of homogeneous material perfectly centered in the rabbit tube.
4. The rabbit moves only in the upward direction when it does move.
5. The initial temperature map for the model is known.
6. No radial temperature gradient exists in either of the two water systems.
7. Radiative heat transfer is neglected.
8. One-dimensional heat transfer is by conduction and convection in the radial direction.
9. Heat transfer occurs in the time interval while all water and rabbit motion is "frozen."
10. Heat transport\* for a time interval occurs in one finite, discrete "jump"; i.e., time is "frozen."
11. The radial boundary of the ITC water cell is perfectly insulated; i.e., there is no heat transfer through the boundary.
12. Solid-material properties are invariant with temperature.
13. Water properties are temperature-dependent.
14. The nodal array is fixed in space.

The basic equations used in the analysis are as follows:

For time-dependent, one-dimensional (radial) heat conduction,

$$\frac{\partial^2 T}{\partial r^2} + \frac{1}{r} \frac{\partial T}{\partial r} + \frac{Q}{k} = \frac{\rho c}{k} \frac{\partial T}{\partial t}. \quad (1)$$

For time-dependent heat balances in the two water zones,

$$hA(T_{bw} - T_W) + q = \rho Vc \frac{dT_{bw}}{dt}. \quad (2)$$

With reference to Fig. 3, radial nodes are fixed at eight, with No. 1 to 3 existing only in the rabbit, No. 4 being the rabbit coolant node, No. 5 to 7 the nodes in the rabbit-tube wall, and No. 8 the ITC coolant node. Radial nodes in the rabbit and rabbit-tube wall are equally spaced, but not necessarily at the same intervals in both.

---

\*Heat transfer due to movement of heated bodies of matter.

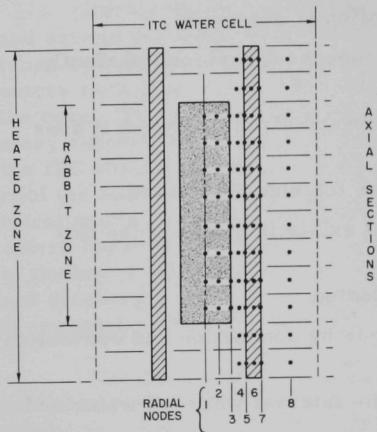


Fig. 3. Nodal Array Used in Analysis of One Hydraulic Rabbit Assembly

In the axial direction, the nodes are located at the center of equal-length sections into which the heated zone is divided. These sections, in turn, are separated into two groups: rabbit-free and rabbit-affected.

### C. Transient Heat-balance Equations

#### 1. Heat Transfer in the Stationary Mode ("Frozen" Motion)

Following the nodal arrangement and the method of Dusinberre,<sup>2</sup> detailed finite-difference equations are derived (from Eqs. 1 and 2) that describe the heat balance for the radial nodes in each of the rabbit-free and rabbit-affected axial sections.

##### a. Rabbit-free Sections (Nodes No. 4 to 8)

###### Node No. 4

$$\frac{2(T_5^{\circledcirc} - T_4^{\circledcirc})}{r_5^2} + \frac{Q_w}{h_5 r_5} = \frac{\rho_w c_w}{h_5 r_5} \frac{T_4^{\circledcirc} - T_4^{\circledcirc}}{\Delta t} \quad (3)$$

###### Node No. 5

$$\frac{8h_5r_5(T_4^{\circledcirc} - T_5^{\circledcirc})}{k_m \Delta r_5(4r_5 + \Delta r_5)} + \frac{4(2r_5 + \Delta r_5)(T_6^{\circledcirc} - T_5^{\circledcirc})}{(\Delta r_5)^2(4r_5 + \Delta r_5)} + \frac{Q_m}{k_m} = \frac{\rho_m c_m}{k_m \Delta t} (T_5^{\circledcirc} - T_5^{\circledcirc}) \quad (4)$$

###### Node No. 6

$$\frac{(2r_6 - \Delta r_6)(T_5^{\circledcirc} - T_6^{\circledcirc})}{2r_6(\Delta r_6)^2} + \frac{(2r_6 + \Delta r_6)(T_7^{\circledcirc} - T_6^{\circledcirc})}{2r_6(\Delta r_6)^2} + \frac{Q_m}{k_m} = \frac{\rho_m c_m}{k_m \Delta t} (T_6^{\circledcirc} - T_6^{\circledcirc}) \quad (5)$$

###### Node No. 7

$$\frac{4(2r_7 - \Delta r_6)(T_6^{\circledcirc} - T_7^{\circledcirc})}{(\Delta r_6)^2(4r_7 - \Delta r_6)} + \frac{8h_7r_7(T_8^{\circledcirc} - T_7^{\circledcirc})}{k_m (\Delta r_6)(4r_7 - \Delta r_6)} + \frac{Q_m}{k_m} = \frac{\rho_m c_m}{k_m \Delta t} (T_7^{\circledcirc} - T_7^{\circledcirc}) \quad (6)$$

Node No. 8

$$\frac{2(T_7^{\circledcirc} - T_8^{\circledcirc})}{r_8^2 - r_7^2} + \frac{Q_w}{h_7 r_7} = \frac{\rho_w c_w}{h_7 r_7 \Delta t} (T_8^{\circledcirc} - T_8^{\circledcirc}) \quad (7)$$

b. Rabbit-affected Sections (Nodes No. 1 to 8)Node No. 1

$$\frac{4(T_2^{\circledcirc} - T_1^{\circledcirc})}{(\Delta r_1)^2} + \frac{Q_m}{k_m} = \frac{\rho_m c_m}{k_m \Delta t} (T_1^{\circledcirc} - T_1^{\circledcirc}) \quad (8)$$

Node No. 2

$$\frac{2r_2 - \Delta r_1}{2r_2(\Delta r_1)^2} (T_1^{\circledcirc} - T_2^{\circledcirc}) + \frac{2r_2 + \Delta r_2}{2r_2(\Delta r_1)^2} (T_3^{\circledcirc} - T_2^{\circledcirc}) + \frac{Q_m}{k_m} = \frac{\rho_m c_m}{k_m \Delta t} (T_2^{\circledcirc} - T_2^{\circledcirc}) \quad (9)$$

Node No. 3

$$\begin{aligned} & \frac{4(2r_3 - \Delta r_2)}{(\Delta r_2)^2(4r_3 - \Delta r_2)} (T_2^{\circledcirc} - T_3^{\circledcirc}) + \frac{8h_3 r_3}{k_m \Delta r_2 (4r_3 - \Delta r_2)} (T_4^{\circledcirc} - T_3^{\circledcirc}) + \frac{Q_m}{k_m} = \\ & \frac{\rho_m c_m}{k_m \Delta t} (T_3^{\circledcirc} - T_3^{\circledcirc}) \end{aligned} \quad (10)$$

Node No. 4

$$\begin{aligned} & \left( \frac{2}{r_5^2 - r_3^2} \right) \left[ \frac{h_3 r_3 (T_3^{\circledcirc} - T_4^{\circledcirc}) + h_5 r_5 (T_5^{\circledcirc} - T_4^{\circledcirc})}{h_3 r_3 + h_5 r_5} \right] + \frac{Q_w}{h_3 r_3 + h_5 r_5} = \\ & \frac{\rho_w c_w (T_4^{\circledcirc} - T_4^{\circledcirc})}{(h_3 r_3 + h_5 r_5) \Delta t} \end{aligned} \quad (11)$$

Nodes No. 5 to 8

Equations for Nodes No. 5 to 8 are the same as Eqs. 4 to 7, respectively. The values of all  $T_i^{\circledcirc}$  terms in Eqs. 3 to 11 are the simple averages of the beginning-of-interval and end-of-interval temperatures; i.e.,

$$T_i^{\circledcirc} = \frac{T_i^{\circledcirc} + T_i^{\circledcirc}}{2}. \quad (12)$$

When Eq. 12 is substituted into Eqs. 3 to 11, the only unknowns are the end-of-interval node temperatures. These temperatures are obtained by simultaneous solution of the appropriate sets of equations for each axial section. Since it is assumed that no axial heat transfer takes place, each axial section can be treated independently within each time interval. Also, since the solution is implicit, no iterating is involved and no restriction need be placed on geometric parameters or duration of the time interval. The solution will not "blow up" because of a large geometrical increment or a long time interval; however, a degree of accuracy could be sacrificed for large input values in either case.

## 2. Heat Transfer in the Moving Mode ("Frozen" Time)

As mentioned earlier, heat transfer is assumed to occur in the time interval while all water and rabbit motion is "frozen." However, before the heat transfer is calculated, all heat transport for that time interval is allowed to take place in one finite, discrete "jump"; i.e., time is "frozen." Also, water expansion caused by heating is allowed to occur in the direction of water flow.

Since all nodes are fixed in space, the node temperatures must be adjusted according to the amount of travel of the water and the rabbit. These adjusted temperatures are then used as the beginning-of-interval temperatures for heat-transfer calculations in the next stationary mode ("frozen" motion).

## D. Empirical Formulations

### 1. Heat-transfer Coefficient

The heat-transfer coefficient used in some of the preceding transient heat-balance equations is determined according to the following bulk liquid correlation:<sup>3</sup>

$$h = \frac{0.023 k}{D_h} \left( \frac{D_h G}{\mu} \right)^{0.8} \left( \frac{c_p \mu}{k} \right)^{0.4} . \quad (13)$$

### 2. Water Properties

Water properties in Eq. 13 are temperature-dependent in the following manner:<sup>4</sup>

$$k = 0.3329 + 0.0003148T, \quad (14)$$

$$\mu = 7.695 - 13.88(T/100) + 12.10(T/100)^2 - 5.086(T/100)^3 + 0.8176(T/100)^4, \quad (15)$$

and

$$\begin{aligned} c_p = & 0.9970 + 0.1777(T/1000) - 2.090(T/1000)^2 \\ & + 12.30(T/1000)^3 - 18.33(T/1000)^4. \end{aligned} \quad (16)$$

Temperature-dependent water density (in lb/ft<sup>3</sup>) is given by

$$\begin{aligned} \rho = & 62.20 + 1.270(T/100) - 1.952(T/100)^2 \\ & + 0.5638(T/100)^3 - 0.08217(T/100)^4. \end{aligned} \quad (17)$$

### E. Steady-state Heat-balance Equations

Steady-state equations are obtained by setting  $\Delta T/\Delta t$  equal to zero in Eqs. 3 to 11. These equations can then be solved quite readily without having to adjust node temperatures because of water and rabbit movement.

## IV. METHOD OF SOLUTION

### A. Order of Calculations

Heat transfer in the stationary mode and heat transport in the moving mode are computed for each successive time interval in the following order:

#### 1. Stationary Mode

a. The beginning-of-interval nodal temperature map is known, either being given as input for the first time interval or having been computed from the previous time interval.

b. Temperature-dependent properties are computed for the water in each axial section, using the beginning-of-interval nodal temperature map.

c. The flowrate in each coolant system is computed at the beginning-of-interval time, using straight-line interpolation applied to input values of time-dependent flowrate.

d. Heat-transfer coefficients are determined for each axial section, using Eq. 13.

e. Time- and position-dependent heating rates at the beginning of the time interval are determined for the metal and water in each axial section by straight-line interpolation of the time-dependent and position-dependent heating rates, given as input. The heating rate in the

two coolant systems is, in addition, density-dependent; it is calculated knowing the water density in each axial section.

At this point, all necessary values for the axial section equation sets are known except for the end-of-interval node temperatures. These temperatures are obtained by simultaneous solution of the equation sets, and may be printed out and/or used for calculations during the moving-mode adjustments preparatory to the next time interval.

## 2. Moving Mode

f. The node temperatures are adjusted to account for water flow, water expansion in the direction of flow, and rabbit movement. If the flow is in the normal (downward) direction, the water inlet temperature used is that given as an input value. If the flow is reversed, the water "reverse" inlet temperature is assigned the latest, highest water outlet temperature value determined during flow in the normal direction. These calculations are performed separately and independently for the two coolant systems.

The amount of rabbit movement is determined by straight-line interpolation of input values of rabbit position vs time. Rabbit position is the measured distance between the lower end of the rabbit and the lower end of the heated zone (see Fig. 2).

g. The adjusted node temperatures computed in this manner represent the temperature map input for stationary-mode ("frozen" motion) heat-transfer calculations in the next time interval.

## B. Computer Input

The symbols used in this explanation of the input deck structure are for orderly cataloging only; they do not intentionally correspond to nomenclature used elsewhere in this report. Where appearing, I denotes a fixed-point (integer) input, and X a floating-point input.

<u>Card No.:</u>	<u>I1</u>	<u>Variable:</u>	<u>I1</u>	<u>Format:</u>	<u>I12</u>
	I1 = 0		New problem.		
	= 1		Continue previously completed problem.		
	= 2		Continue previous problem, which was terminated because allowed computer time was exhausted.		

Card No.: 2-5

Format: 4A72

Any title desired. Four cards must be used, even if some are left blank.

<u>Card No.:</u> 6	<u>Variables:</u>	I2, I3, I4, I5, I6, I7	<u>Format:</u>	6I12
	I2	Total number of axial sections ( $\leq 50$ ).		
	I3*	Axial section initially containing lower end of rabbit.		
	I4*	Axial section initially containing upper end of rabbit.		
	I5	Total number of pairs of values ( $\leq 50$ ) for normalized (to value at time zero) heat-generation rate vs time.		
	I6	Total number of pairs of values ( $\leq 50$ ) for normalized (to value at time zero) rabbit-tube flowrate vs time.		
	I7	Total number of pairs of values ( $\leq 50$ ) for rabbit position vs time.		
<u>Card No.:</u> 7	<u>Variables:</u>	I8, I9, I10, I11, I12, I13	<u>Format:</u>	6I12
	I8 = 0	Debug option is activated, and many quantities are printed as they are computed (not normally used for production runs).		
	= 1	Debug option is suppressed.		
	I9 = -1	All initial node temperatures have a single value (X12 in the following).		
	= 1	All initial node temperatures are read in point by point (X23 in the following).		
	I10 = 0	Initial node temperatures (X12 or X23) are overridden by a steady-state calculation which determines the steady-state temperature map of the model.		
	= 1	Steady-state calculation is bypassed.		
	I11 = 0	Problem is terminated after printout of steady-state temperature map.		
	= 1	Problem continues following printout of steady-state temperature map.		
	I12	Compute/print ratio for the temperature map.		
	I13	Total number of pairs of values ( $\leq 50$ ) for normalized (to value at time zero) primary flow vs time.		

\*If the end of rabbit does not extend more than halfway into section, then the section is to be considered rabbit-free.

<u>Card No.:</u> 8*	<u>Variables:</u> X1a, X1b, X1c, ...	<u>Format:</u> 6E12.5
X1a	Inner-to-outer radii for radial Nodes	
X1b	No. 2 to 8 (in inches).	
X1c		
	.	.
	.	.
<u>Card No.:</u> 9	<u>Variables:</u> X2, X3, X4, X5, X6, X7	<u>Format:</u> 6E12.5
X2	Length of heated zone (in inches).	
X3	Length of rabbit or total length of several rabbits placed end to end (in inches).	
X4	Initial rabbit position (in inches).	
X5	Computation time interval (in seconds).	
X6	Delayed time at which the debug option will be activated if it was not activated initially (in seconds).	
X7	Problem termination time (in seconds).	
<u>Card No.:</u> 10	<u>Variables:</u> X8, X9, X10, X11	<u>Format:</u> 4E12.5
X8	Initial axial-position-dependent peak heating rate in the water systems (in W/g).	
X9	Initial axial-position-dependent peak heating rate in the metal (in W/g).	
X10	Initial mass flowrate in the open rabbit tube (in lb/(hr)(ft <sup>2</sup> )).	
X11	Initial mass flowrate in the primary water cell (in lb/(hr)(ft <sup>2</sup> )).	
<u>Card No.:</u> 11	<u>Variables:</u> X12, X13, X14, X15, X16, X17	<u>Format:</u> 6E12.5
X12	Constant temperature value for the initial node temperatures (in °F).	
X13	Bulk water inlet temperature for the tube water (in °F).	
X14	Bulk water inlet temperature for the primary water cell (in °F).	
X15	Metal conductivity (in Btu/(hr)(ft)(°F)).	
X16	Metal density (in lb/ft <sup>3</sup> ).	
X17	Metal specific heat (in Btu/(lb)(°F)).	

\*Continuation onto one more card is necessary.

<u>Card No.:</u>	<u>12*</u>	<u>Variables:</u>	X18a, X18b, X18c, ...	<u>Format:</u>	6E12.5
		X18a	Initial normalized (to maximum value) axial		
		X18b	heat-generation profile.		
		X18c			
<u>Card No.:</u>	<u>13*</u>	<u>Variables:</u>	X19a, X19b, X19c, ...	<u>Format:</u>	6E12.5
		X19a	Pairs of values for normalized (to value at		
		X19b	time zero) heat-generation rate vs time (in		
		X19c	seconds). Time is given first for each pair.		
<u>Card No.:</u>	<u>14*</u>	<u>Variables:</u>	X20a, X20b, X20c, ...	<u>Format:</u>	6E12.5
		X20a	Pairs of values for normalized (to value at		
		X20b	time zero) rabbit-tube flowrate vs time (in		
		X20c	seconds). Time is given first for each pair.		
<u>Card No.:</u>	<u>15*</u>	<u>Variables:</u>	X21a, X21b, X21c, ...	<u>Format:</u>	6E12.5
		X21a	Pairs of values for normalized (to value at		
		X21b	time zero) primary water cell flowrate vs		
		X21c	time (in seconds). Time is given first for		
			each pair.		
<u>Card No.:</u>	<u>16*</u>	<u>Variables:</u>	X22a, X22b, X22c, ...	<u>Format:</u>	6E12.5
		X22a	Pairs of values for rabbit position (in		
		X22b	inches) vs time (in seconds). Time is		
		X22c	given first for each pair.		

\*Continue on as many cards as necessary.

Card No.: 17\*    Variables: X23a, X23b, X23c, ...    Format: 6E12.5

X23a	If I9 = 1, initial node temperatures (in °F) read in point by point (inner-to-outer radial nodes for each axial section from top to bottom). Dummy filler values must be used in axial sections where radial Nodes No. 1 to 3 do not exist.
X23b	
X23c	

### C. Computer Output

The standard output for a problem consists of:

1. The input data in the order in which it appears on the input cards.
2. A geometric map of the model with the rabbit in its initial position.
3. The input temperature map with node temperatures placed as shown on the geometric map.
4. The overriding steady-state temperature map, if it is computed.
5. Time-dependent temperature maps.

### V. GENERAL APPLICABILITY

The TRANTEMP code probably will find its primary use directed toward determining reactor operating conditions under which boiling might occur in a hydraulic rabbit system. Since the system water is always assumed to be in the liquid state, the onset of boiling, although not "flagged" by the code, can be determined if the system pressure is known, by examining the calculated time-dependent water temperatures.

There is no limit on the range of flowrates that can be used in either the rabbit cooling system or the rabbit-tube cooling system, and these two flowrates are completely independent of each other. Moreover, there is no limit on the heating rate range or on the axial heat-generation profile. Therefore, the consequences of tube-flow blockage can be analyzed.

Any dimensions can be used to fit any given heat-transfer model; the only restriction is that cylindrical geometry must be used.

---

\*Continue on as many cards as necessary.

The TRANTEMP Code can be adapted for use on any computer with a 32k memory that can process coding written in the FORTRAN language. No unusual library functions are required. Finally, because the number of radial nodes (hence, the maximum number of equations requiring simultaneous solution) is fixed at eight, the running time for any problem is almost directly proportional to the number of axial sections and inversely proportional to the duration of the computation time interval. For example, the hypothetical problem analyzed in Appendix A required 138 sec of running time on the CDC-3600 computer.

## APPENDIX A

Sample Problem

The computer input and output displayed in this appendix are illustrative of a hypothetical hydraulic rabbit system problem which can be solved using the TRANTEMP code described in the text.

The input information for the sample problem is reproduced on pages 24 and 25. The listing of the input deck is given on page 26.

Appendix B gives a complete listing of the FORTRAN source deck.

1. Problem Input

The following explanatory comments are made with reference to the input data sheets and the corresponding instructions given in Section IV.B of the text.

Card No. 1. This is a new problem ( $I1 = 0$ ).

Card No. 6. There are 20 equal-length axial sections ( $I2$ ). Axial section No. 4 initially contains the lower end of the rabbit ( $I3$ ). Axial section No. 17 initially contains the upper end of the rabbit ( $I4$ ). There are seven pairs of values ( $I5$ ) for normalized heat-generation rate vs time, seven pairs of values ( $I6$ ) for normalized tube flow vs time, and ten pairs of values ( $I7$ ) for rabbit position vs time.

Card No. 7. The debug option is suppressed ( $I8 = 1$ ). The initial node temperatures all have a single value ( $I9 = -1$ ); however, these temperatures are overridden ( $I10 = 0$ ) by a steady-state temperature map calculation based on time-independent conditions evaluated at time zero. The problem continues following printout of the steady-state temperature map ( $I11 = 1$ ). Every 10th time-dependent temperature map computed is printed out ( $I12 = 10$ ). There are seven pairs of values ( $I13 = 7$ ) for normalized primary flow vs time.

Cards No. 8. The inner-to-outer radii ( $r_2, r_3, \dots, r_8$ ) are, respectively, 0.125, 0.25, 0.28125, 0.3125, 0.34375, 0.375, and 0.5 in. ( $X_{1a}, X_{1b}, \dots, X_{1g}$ ). Radius  $r_1$  is always taken to be zero.

Card No. 9. The length of the heated zone is 27.559 in. ( $X2$ ). The rabbit is 20 in. long ( $X3$ ) and centered in both the radial and axial directions. The bottom of the rabbit is 3.7795 in. above the bottom of the heated zone ( $X4$ ). The computation time interval is 0.01 sec ( $X5$ ). The debug option is to be activated at 10 sec ( $X6$ ); however, since the problem termination time is 4 sec ( $X7$ ), this option will not be activated.

Card No. 10. The maximum initial heating rate is 138 W/g in the two water systems (X8) and 72 W/g in the metal (X9). The initial mass flowrate is  $1.4 \times 10^6 \text{ lb}/(\text{hr})(\text{ft}^2)$  in the open rabbit tube (X10) and  $8.9796 \times 10^5 \text{ lb}/(\text{hr})(\text{ft}^2)$  in the primary water cell (X11).

Card No. 11. The single constant temperature value for the initial node temperatures (X12) is 130°F. The bulk water inlet temperature for both the tube (X13) and primary water (X14) is 120°F. The metal is aluminum, with a conductivity (X15) of 123.12 Btu/(hr)(ft)(°F), density (X16) of 168.512 lb/ft<sup>3</sup>, and specific heat (X17) of 0.215 Btu/(lb)(°F).

Cards No. 12. An assumed sinusoidal axial heat-generation profile over the length of the heated zone is approximated by the 20 normalized node values as given on the input cards.

Cards No. 13. The pairs of values for normalized heat-generation rate vs time are listed in order for the following times: 0.0, 0.25, 0.5, 0.75, 1.0, 2.0, and 5.0 sec.

Cards No. 14. The pairs of values for normalized rabbit-tube flowrate vs time are listed in order for the following times: 0.0, 0.25, 0.5, 0.75, 1.0, 3.0, and 5.0 sec.

Cards No. 15. The pairs of values for normalized primary water cell flowrate vs time are listed in order for the following times: 0.0, 0.25, 0.5, 0.75, 1.0, 3.0, and 5.0 sec.

Cards No. 16. The pairs of values for rabbit position vs time are listed in order for the following times: 0.0, 0.75, 1.0, 1.1, 1.2, 1.3, 1.4, 2.0, 3.0, and 5.0 sec. The rabbit must not proceed in a reverse direction at a rate greater than the reverse rabbit-tube water flow (values given on Cards No. 14). If input is inadvertently submitted so that this situation occurs, a diagnostic message will be printed and the problem terminated.

Cards No. 17. Since I9 = -1, this set of cards is omitted.

## 2. Problem Output

The output for the sample problem is reproduced on pages 27 to 60.

## INPUT DATA

## INPUT DATA

## LISTING OF INPUT DECK

```

0 *****TITLE1*****TITLE2*****TITLE3*****TITLE4*****CARD 1
*****CARD 2
*****CARD 3
*****CARD 4
*****CARD 5
20      4       17      7       7      10CARD 6
1      -1       0       1      10      7CARD 7
.125     .25     .28125     .3125     .34375     .375CARD 8A
.5
27.559    20.    3.7795     .01      10.      4.CARD 9
138.     72.    1.4E+6   8.9796E+5
130.     120.    120.    123.12    168.512    .215CARD 11
.07846    .23345   .38268   .52250   .64945   .76041CARD 12A
.85264    .92388   .97237   .99592   .99692   .97237CARD 12B
.92388    .85264   .76041   .64945   .52250   .38268CARD 12C
.23345    .07846
0.        1.      .25      .99      .5      .975CARD 13A
.75      .925      1.      .85      2.      .53CARD 13B
5.        .5
0.        1.      .25      .5      .5      0.CARD 14A
.75      -.5      1.      -1.      3.      -1.CARD 14B
5.        -1.
0.        1.      .25      .5      .5      0.CARD 15A
.75      -.5      1.      -1.      3.      -1.CARD 15B
5.        -1.
0.        3.7795     .75     3.7795     1.      13.CARD 16A
1.1      17.      1.2      21.      1.3      25.CARD 16B
1.4      30.      2.      35.      3.      37.CARD 16C
5.        38.

```

INPUT INFORMATION

\*\*\*\*\*TITLE1\*\*\*\*\*  
 \*\*\*\*\*TITLE2\*\*\*\*\*  
 \*\*\*\*\*TITLE3\*\*\*\*\*  
 \*\*\*\*\*TITLE4\*\*\*\*\*

CARD 6\*\*\* TOTAL AXIAL AXIAL SECTION AXIAL SECTION TOTAL NUMBER OF NORMALIZED TOTAL NUMBER OF TOTAL NUMBER OF  
 SECTIONS CONTAINING CONTAINING TOP HEAT GENERATION RATE NORMALIZED TUBE RABBIT POSITION  
 BOTTOM END OF END OF VERSUS TIME PAIRS FLOW VERSUS TIME VERSUS TIME  
 RABBIT SAMPLE RABBIT SAMPLE OF VALUES PAIRS OF VALUES PAIRS OF VALUES  
 20 4 17 7 7 10

CARD 7\*\*\* DEBUG OPTION OPTION FOR INITIAL STEADY-STATE STEADY-STATE COMPUTE/PRINT TOTAL NUMBER OF  
 (INITIAL) TEMPERATURE MAP COMPUTATION OPTION TERMINATE OPTION FREQUENCY NORMALIZED PRIMARY  
 FLOW VERSUS TIME PAIRS  
 1 -1 0 1 10 7  
 OF VALUES

CARDS 8\*\*\* INNER-TO-OUTER RADII (INCHES)  
 FIRST SECOND THIRD FOURTH FIFTH SIXTH SEVENTH EIGHTH  
 0.0000 0.1250 0.2500 0.2813 0.3125 0.3438 0.3750 0.5000

CARD 9\*\*\* HEATED LENGTH OF LENGTH OF DISTANCE BETWEEN COMPUTATION TIME STARTING TIME FOR PROBLEM  
 RABBIT TUBE RABBIT SAMPLE LOWER END OF RABBIT INTERVAL DELAYED DEBUG TERMINATION  
 (INCHES) (INCHES) AND LOWER END OF HEATED (SECONDS) (SECONDS) (SECONDS)  
 27.5590 20.0000 3.7795 0.0100 10.0000 4.0000

CARD 10\*\*\* MAXIMUM, INITIAL MAXIMUM, INITIAL INITIAL MASS FLOW INITIAL MASS FLOW  
 HEATING RATE IN HEATING RATE IN IN THE OPEN RABBIT TUBE IN THE PRIMARY  
 WATER (WATTS/GM) METAL (WATTS/GM) {LB/HR-SQ. FT} {LB/HR-SQ. FT}  
 138.0000 72.0000 1400000.0000 897960.0000

CARD 11\*\*\* TEMPERATURE VALUE TUBE WATER INLET PRIMARY WATER INLET METAL METAL METAL SPECIFIC  
 FOR CONSTANT TEMPERATURE TEMPERATURE TEMPERATURE CONDUCTIVITY DENSITY HEAT  
 MAP (DEGREE F) (DEGREE F) (DEGREE F) (BTU/HR-FT-DEGREE F) (PCF) (BTU/LB-DEGREE F)  
 130.0000 120.0000 120.0000 123.1200 168.5120 0.2150

CARDS 12\*\*\*NORMALIZED AXIAL HEAT GENERATION PROFILE

AXIAL POSITION	NORMALIZED HEAT GENERATION RATE
1	0.0785
2	0.2334
3	0.3827
4	0.5225
5	0.6494
6	0.7604
7	0.8526
8	0.9239
9	0.9724
10	0.9969
11	0.9969
12	0.9724
13	0.9239
14	0.8526
15	0.7604
16	0.6494
17	0.5225
18	0.3827
19	0.2334
20	0.0785

CARDS 13\*\*\*NORMALIZED HEAT GENERATION RATE VERSUS TIME

TIME (SECONDS)	NORMALIZED HEAT GENERATION RATE
0.0000	1.0000
0.2500	0.9900
0.5000	0.9750
0.7500	0.9250
1.0000	0.8500
2.0000	0.5300
5.0000	0.5000

CARDS 14\*\*\*NORMALIZED RABBIT TUBE FLOW RATE VERSUS TIME

TIME (SECONDS)	NORMALIZED FLOW RATE
0.0000	1.0000
0.2500	0.5000
0.5000	0.0000
0.7500	-0.5000
1.0000	-1.0000
3.0000	-1.0000
5.0000	-1.0000

CARDS 15\*\*\*

NORMALIZED PRIMARY FLOW RATE VERSUS TIME

TIME (SECONDS)	NORMALIZED FLOW RATE
0.0000	1.0000
0.2500	0.5000
0.5000	0.0000
0.7500	-0.5000
1.0000	-1.0000
3.0000	-1.0000
5.0000	-1.0000

CARDS 16\*\*\*

RABBIT POSITION VERSUS TIME

TIME (SECONDS)	RABBIT POSITION (INCHES)
0.0000	3.7795
0.7500	3.7795
1.0000	13.0000
1.1000	17.0000
1.2000	21.0000
1.3000	25.0000
1.4000	30.0000
2.0000	35.0000
3.0000	37.0000
5.0000	38.0000

### COMPUTED OUTPUT

THE INITIAL CONDITION GEOMETRICAL ARRANGEMENT FOR THIS PROBLEM IS DESCRIBED IN THE FOLLOWING DIAGRAM. \*\*\*\*\* (ALL DIMENSIONS ARE IN INCHES.)

RADIUS *	(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
0.0000	0.1250	0.2500	0.2813	0.3125	0.3438	0.3750	0.5000	
Z								
(20) 26.8700			X	X	X	X	X	X
(19) 25.4921			X	X	X	X	X	X
(18) 24.1141			X	X	X	X	X	X
(17) 22.7362	X	X	X	X	X	X	X	X
(16) 21.3582	X	X	X	X	X	X	X	X
(15) 19.9803	X	X	X	X	X	X	X	X
(14) 18.6023	X	X	X	X	X	X	X	X
(13) 17.2244	X	X	X	X	X	X	X	X
(12) 15.8464	X	X	X	X	X	X	X	X
(11) 14.4685	X	X	X	X	X	X	X	X
(10) 13.0905	X	X	X	X	X	X	X	X
( 9) 11.7126	X	X	X	X	X	X	X	X
( 8) 10.3346	X	X	X	X	X	X	X	X
( 7) 8.9567	X	X	X	X	X	X	X	X
( 6) 7.5787	X	X	X	X	X	X	X	X
( 5) 6.2008	X	X	X	X	X	X	X	X
( 4) 4.8228	X	X	X	X	X	X	X	X
( 3) 3.4449			X	X	X	X	X	X
( 2) 2.0669			X	X	X	X	X	X
( 1) 0.6890			X	X	X	X	X	X

TIME (SECONDS)

TEMPERATURE MAP (DEGREE F)

THE INITIAL CONDITION, STEADY-STATE TEMPERATURE MAP\*\*\*\*\*

150.1053	147.9388	141.4394	120.1111	122.6490	122.6949	122.6590	122.1685
158.0389	155.3460	147.2675	120.4420	128.0087	128.1460	128.0399	120.6694
165.2591	162.1062	152.6474	121.9948	130.0436	130.6333	130.6537	122.4881
171.5906	168.0553	157.4493	123.2134	133.4343	133.6609	133.4884	121.4897
176.8867	173.0560	161.5638	121.0136	133.4343	133.6609	133.4884	121.4897
181.0300	176.9982	164.9229	126.2378	136.1915	137.0453	137.0708	125.1833
183.9354	179.8018	167.4111	127.9708	144.2576	145.3477	145.3789	130.4341
185.5494	181.4159	169.0151	121.9948	131.6580	146.3879	147.5058	132.3360
185.8506	181.8188	169.7235	123.4301	133.5249	148.1571	149.2758	134.2363
184.8484	181.1176	169.5254	124.6395	135.3456	149.5295	150.6217	136.0881
182.5886	179.0453	168.4392	126.3278	137.0756	150.4781	151.5175	137.8458
179.1125	175.9596	166.5008	127.9591	138.6723	150.9854	151.9468	139.4661
174.5327	171.8399	163.7614	128.0287	140.0969	151.0427	151.9028	151.9341
168.9530	166.7865	160.2871	129.7908	141.3144	150.6502	151.3883	142.1397
				142.2951	149.8172	150.4155	150.4436
				142.8377	154.5697	154.8076	154.6454
				143.1720	150.6023	150.7578	150.6684
				143.2892	146.2100	146.2780	144.2622
							144.5838

0.0100

150.1058	147.9423	141.4965	120.1719	122.6508	122.6959	122.6606	120.2277
158.0395	155.3503	147.3887	120.6231	128.0139	128.1489	128.0447	120.8453
165.2599	162.1113	152.7312	121.3265	133.4432	133.6658	133.4962	121.7778
171.5915	168.0610	157.5438	123.4301	130.1486	130.6709	130.6812	122.8389
176.8876	173.0622	161.6668	124.9962	132.2783	133.9247	133.9352	124.1660
181.0310	177.0048	165.0120	125.3456	136.7260	136.3456	137.1004	137.1112
183.9364	179.8086	157.5138	126.4395	134.3921	142.9148	142.9264	129.1987
185.5514	181.4227	169.1286	127.0206	136.2392	144.5194	145.4315	131.0877
185.8516	181.8255	169.8449	128.0129	136.3292	148.3656	149.3503	133.0059
184.8493	181.0240	169.6320	128.0129	138.0129	149.3731	149.3634	134.9060
182.5815	179.0512	168.5382	129.6104	136.1915	150.6949	150.7085	136.7411
179.1133	175.9549	166.5895	130.0125	151.1671	151.5875	151.6018	138.4659
174.5334	171.8445	163.8375	142.1850	151.2056	152.0117	152.0267	140.0380
168.9535	166.7902	160.3487	143.7331	150.7901	151.9610	151.9768	141.4187
				143.1829	149.9302	151.4383	151.4548
				143.3560	150.4558	150.4732	142.5743
				143.3537	146.2120	146.2790	143.4762
							144.2229
							144.5991
							144.6396

0.1000

150.2276	148.1692	142.1474	120.1284	122.7208	122.7609	122.7297	120.1929
158.1862	155.6265	148.1456	120.5067	128.2291	128.3492	128.2571	120.7624
165.4565	162.4688	153.7331	123.7745	133.6624	134.3323	133.8437	121.6897
171.8257	168.4815	158.7040	125.4103	136.8676	137.6475	134.3654	124.2155
177.1595	173.5437	162.9696	127.2031	139.9088	140.7789	137.6841	125.8208
181.3336	177.5360	166.4278	131.1257	142.7468	143.6858	140.8182	127.5902
184.2641	180.3795	169.0142	133.1540	145.3039	146.2886	143.7271	129.4786
185.8957	182.1209	170.6820	135.1602	147.5287	148.5348	146.5770	133.4219
186.2067	182.4384	171.4100	137.0933	150.7965	151.7708	150.4157	135.3770
185.2059	181.6383	171.1974	138.9195	151.7742	152.6959	151.8101	137.2556
182.3313	179.6532	170.0638	140.5902	152.2871	153.1324	152.7322	139.0112
179.4481	176.5411	168.0462	142.0961	152.3267	153.0719	153.1644	140.6008
174.8455	172.3817	165.1960	143.3955	151.8923	152.5152	153.0980	141.9851
169.2357	167.2763	161.5796	144.4288	150.9904	151.4732	151.4834	144.0083
			144.8668	155.2698	155.4446	155.2980	144.6870
			145.1562	151.1154	151.2149	151.1303	145.0278
			145.0501	146.5134	146.5373	146.5168	145.0236

0.2000

150.9616	149.1438	143.8941	120.1599	122.9369	122.9712	122.9447	120.2356
159.1137	156.8633	150.3689	120.6256	128.8787	128.9812	128.9031	120.9165
166.5698	163.9429	156.3644	121.2890	134.8602	135.0302	134.9047	121.9914
173.0978	170.1608	161.6922	127.9443	142.0045	142.7628	142.8004	128.5588
178.5634	175.3895	166.2420	130.1001	145.0740	145.8873	145.9255	130.6188
182.8376	179.5060	169.9087	132.3331	147.8135	148.6608	148.6986	132.7315
185.8346	182.4282	172.6210	134.5835	150.1642	151.0237	151.0600	134.8395
187.4975	184.1014	174.3297	136.7914	152.0743	152.9241	152.9576	136.8881
187.8046	184.5036	175.0124	138.8986	153.5046	154.3229	154.3528	138.8252
186.7654	183.6422	174.6697	140.8497	154.4267	155.1925	155.2179	140.6023
184.4191	181.5521	173.3242	142.5938	154.8231	155.5170	155.5371	142.1752
180.8332	178.2946	171.0188	144.0854	154.6878	155.2921	155.3064	143.5049
176.0995	173.9535	167.8140	145.2585	154.0250	154.5242	154.5323	144.5587
170.3332	168.6344	163.7872	146.1641	152.8496	153.2312	153.2327	145.3107
			146.2935	156.7272	156.8651	156.7434	145.8343
			146.1060	152.1465	152.2265	152.1584	145.9847
			145.7916	147.1065	147.1235	147.1089	145.7617

0.3000

152.5934	151.0685	146.7401	120.2140	123.3002	123.3280	123.3067	120.3090
161.1775	159.2929	153.9461	120.8270	129.9706	130.0534	129.9909	121.1841
169.0162	166.8190	160.5880	121.6912	136.6647	136.8017	136.7016	122.5294
175.8748	173.4217	166.4683	123.2441	133.6916	134.0906	134.1156	124.1121
181.6074	178.9606	171.4616	127.2779	141.8442	142.4067	142.4371	128.0712
186.0794	183.3061	175.4532	132.1254	149.0694	149.7339	149.7653	132.6393
189.1998	186.3705	178.3639	134.6808	152.1058	152.7948	152.8249	134.9843
190.9094	188.0961	180.1408	137.2282	154.6616	155.3567	155.3843	137.2813
191.1854	188.4600	180.7601	142.0195	158.1179	158.7696	158.7892	141.4829
190.0385	187.4706	180.2244	144.1336	158.9467	159.5500	159.5641	143.2768
187.5108	185.1661	178.5607	145.9832	159.1502	159.6888	159.6987	144.8030
183.6741	181.6128	175.8189	147.5179	158.7255	159.1848	159.1859	146.0230
178.6260	176.9011	172.0685	148.6940	157.6820	158.0496	158.0435	146.9066
172.4890	171.1447	167.3981	149.4764	156.0421	156.3081	156.2947	147.4317
			149.2901	159.1218	159.2122	159.1140	147.6809
			148.6686	153.7917	153.8368	153.7817	147.5067
			147.8213	147.9665	147.9633	147.9513	146.9177

0.4000

155.3165	154.1589	151.0139	120.3199	123.8481	123.8668	123.8526	120.4429
164.6008	163.1729	159.2960	121.2037	131.6137	131.6694	131.6278	121.6506
173.0591	171.3975	166.8886	122.4222	139.3792	139.4709	139.4045	123.4260
180.4473	178.5957	173.5736	124.4492	136.9812	137.2802	137.2785	125.4647
186.6040	184.6100	179.2049	128.6886	141.9858	142.3248	142.3452	127.8038
191.3852	189.3006	183.6529	132.4546	146.7879	147.1772	147.1987	130.3472
194.6928	192.5714	186.8284	134.2435	151.2435	151.6716	151.6932	133.0065
196.4637	194.3608	188.6727	135.4588	155.2484	155.7032	155.7239	135.6991
196.6742	194.6447	189.1610	138.5040	158.7037	159.1726	159.1914	138.3457
199.3371	193.4340	188.2994	141.4702	161.5306	162.0004	162.0163	140.8713
192.4988	190.7723	186.1227	144.2808	163.6653	164.1229	164.1352	143.2053
188.2385	185.7339	182.6923	146.8545	165.0619	165.4946	165.5025	145.2841
182.6628	181.4197	178.0932	149.1175	165.6916	166.0873	166.0902	147.0521
175.9057	174.9566	172.4325	151.0051	165.5422	165.8899	165.8874	148.4628
			153.4514	162.9395	163.1639	163.1499	150.0778
			153.9400	160.5420	160.6945	160.6748	150.2408
			153.0737	162.4733	162.5211	162.4545	150.0646
			151.6794	156.0361	156.0555	156.0182	149.3995
			150.1494	149.0553	149.0435	149.0350	148.2696

0.5000

159.5284	158.9133	157.6179	120.5808	124.6881	124.6906	124.6888	120.7299
169.8693	169.1118	167.5164	122.0425	134.1209	134.1284	134.1230	122.5639
179.2591	178.3787	176.5247	123.9576	143.5034	143.5156	143.5071	125.0273
187.4339	186.4538	184.3900	129.9778	142.4078	142.4502	142.4559	127.7355
194.2117	193.1575	190.9376	133.4193	154.7694	148.8213	148.8279	130.7175
199.4347	198.3340	196.0164	136.9956	160.2343	160.2993	160.3069	137.0168
202.9942	201.8761	199.5220	140.6053	165.0343	165.1035	165.1111	140.1270
204.8221	203.7161	201.3884	144.1251	169.0515	169.1228	169.1302	143.0870
204.8938	203.8295	201.5905	147.4531	172.1931	172.2646	172.2715	145.8134
203.2257	202.2316	200.1418	150.4906	174.3880	174.4575	174.4637	148.2303
199.8722	198.9751	197.0910	153.1482	175.5866	175.6543	175.6595	150.2718
194.9242	194.1481	192.5204	155.3479	175.7707	175.8307	175.8347	151.8830
188.5038	187.8694	186.5417	158.1307	173.0543	173.1379	173.1391	153.6557
180.7635	180.2876	179.2947	158.6306	170.2970	170.3305	170.3301	153.7703
			158.5083	166.6023	166.6249	166.6229	153.3610
			156.6983	166.9370	166.9425	166.9331	152.5424
			154.1385	158.8635	158.8656	158.8603	151.1664
			151.7000	150.1833	150.1813	150.1798	149.2796

0.6000

165.3111	164.8203	163.0296	122.1960	125.5355	125.5505	125.5371	122.0594
177.6675	176.4539	174.1925	125.1074	136.5887	136.6426	136.5978	125.0242
187.6971	186.0757	184.2983	129.8516	147.5653	147.6472	147.5696	128.4551
196.9071	196.0964	193.0715	138.1333	147.7457	147.9234	147.8942	132.0125
204.4903	203.6113	200.3170	142.8254	155.3553	155.5949	155.5621	135.7691
210.2698	209.3457	205.8695	147.4114	162.4421	162.7375	162.7014	139.5383
214.1243	213.1800	209.6156	151.7517	168.8100	169.1530	169.1140	143.1996
215.9790	215.0401	211.4848	155.7170	174.3071	174.6884	174.6472	146.6449
215.8091	214.9013	211.4928	160.0673	178.8000	179.2091	179.1662	149.7766
213.5373	212.7854	209.5380	164.2647	182.1854	182.6111	182.5673	152.5081
209.5298	208.7570	205.7987	165.7169	184.3871	184.8177	184.7738	154.7648
203.5951	202.9221	200.3422	165.3810	185.3576	185.7814	185.7383	156.4856
195.9783	195.4232	193.2731	167.0004	185.0779	185.4834	185.4420	157.6240
186.8612	186.4404	184.7993	166.2423	183.5563	183.9326	183.8939	158.1493
			165.3370	180.8299	181.1661	181.1307	158.0470
			163.8088	176.9662	177.2501	177.2177	157.3215
			161.9579	172.0715	172.2865	172.2550	156.0131
			157.8004	171.2196	171.2848	171.2031	154.2172
			154.2646	161.5555	161.5894	161.5422	151.8620
			151.9893	151.2725	151.2635	151.2512	149.6369

0.7000

170.3430	169.7911	168.5390	151.7281	126.5793	126.5089	126.4890	126.3737
183.1343	182.2947	180.0240	156.7474	138.6379	138.5689	138.4746	130.6840
194.6456	193.5363	190.2959	155.0011	150.8528	150.7426	150.5583	135.1467
204.5685	203.2173	199.0793	174.7806	153.0551	154.4208	154.1006	139.5693
212.6813	211.1233	206.2009	177.8622	170.3931	170.0788	162.2872	144.0145
218.7982	217.0760	211.5056	179.8512	176.7912	176.6286	169.7618	148.2449
222.7928	220.9543	214.8955	180.4893	182.1117	182.1069	181.8267	155.5829
224.5888	222.6865	216.3185	179.2122	186.2342	186.3875	186.1367	158.4874
224.1642	222.2534	215.7721	177.0594	190.5900	191.0312	190.8539	162.3756
221.5458	219.6869	213.3015	174.2516	190.7675	191.3207	191.1825	163.2943
216.8210	215.0670	208.9964	171.0423	189.6369	190.2687	190.1670	163.3847
210.1087	208.5222	202.9897	167.6860	183.7374	184.3979	184.3492	161.4190
201.5841	200.2252	195.4537	164.4175	179.1905	179.7934	179.7568	159.4102
191.4656	190.3936	186.6000	161.4419	173.7782	174.2746	174.2391	156.8636
			155.6304	173.1178	173.2813	173.1258	154.0380
			153.0523	162.8499	162.9370	162.8410	151.3475
			151.8930	152.1614	152.1550	152.1267	149.6532

0.8000

178.4067	178.4901	178.8537	162.7502	131.3164	130.7009	130.5830	135.3138
189.6943	189.3433	188.3926	171.5330	144.3317	143.7489	143.5311	140.7253
201.1053	200.2195	197.5453	184.0984	168.7694	167.5931	166.9906	150.9930
210.7940	209.4008	205.0981	187.1808	175.8363	174.9220	174.3554	155.6086
218.5428	216.6928	210.9225	189.0512	181.8345	181.2007	180.6826	159.6984
224.1970	221.9587	214.9419	189.4538	186.6528	186.3048	185.8448	163.1510
227.6538	225.1120	217.1227	188.1277	190.2324	190.1522	189.7661	165.8743
228.8648	226.1174	217.4704	185.9508	192.5511	192.7379	192.4077	167.7963
227.8333	224.9872	216.0249	183.0719	193.6220	194.0338	193.7675	168.8672
224.6136	221.7800	212.8577	179.7182	194.4851	194.0807	193.8726	169.0610
219.3082	216.5989	208.0702	172.2022	190.9335	192.7750	168.3784	
212.6668	209.5898	201.7883	175.9870	189.8515	190.6670	190.5476	166.8539
203.3043	201.1451	194.3114	171.9806	186.5197	187.3715	187.2810	164.5700
193.7892	191.9899	186.2085	167.5468	182.2833	183.1425	183.0768	161.6841
			162.7386	177.2405	178.0757	178.0353	158.4632
			155.2255	172.8967	173.1778	172.9461	155.2963
			153.6773	172.5849	172.8330	172.6094	152.6129
			152.4181	162.7334	162.8613	162.7204	150.6124
			151.7898	152.7006	152.7002	152.6534	149.5258

0.9000

189.0517	188.7005	187.8036	185.3416	152.8347	149.8657	148.9468	149.6139
199.1597	198.4005	196.2363	190.3123	166.693	163.7652	162.9056	165.4017
208.7306	207.4710	203.7649	193.7545	176.4965	174.7918	174.0003	160.5848
216.8109	215.7594	210.8353	195.7450	182.8587	181.5525	180.8320	165.0525
222.9605	220.7788	214.2226	196.5050	187.9619	187.0598	186.4208	168.7519
227.0313	224.5014	216.8566	196.0720	191.8346	191.3364	190.7883	171.5883
228.9751	226.1909	217.7337	194.4849	194.4486	194.3433	193.8864	173.4909
228.7895	225.8527	216.8806	191.7396	195.8109	196.0782	195.7155	174.4166
226.5203	223.5350	214.3536	188.1051	195.9558	196.5655	196.2949	174.3528
222.2800	219.3463	210.2554	183.5688	194.9479	195.8564	195.6718	173.3241
216.3212	213.5251	204.7945	178.4379	192.8761	194.0254	193.9182	171.4037
209.1910	206.5879	198.4033	173.0388	189.8561	191.1779	191.1292	168.7288
202.1107	199.7009	192.0715	167.5412	185.9835	187.4022	187.4034	165.5158
197.7984	195.5016	188.1367	163.6113	181.6610	183.0148	183.0286	162.0630
			158.0522	180.4744	180.8851	180.5661	158.7174
			155.5374	177.0441	177.4146	177.1163	155.7449
			154.0411	172.5166	172.8261	172.5545	153.3081
			152.9913	170.2976	170.5807	170.3117	151.4746
			152.2094	151.6124	161.7573	161.5870	150.1691
			151.7524	152.8888	152.8918	152.8289	149.4404

1.0000

210.6521	209.1669	204.6721	193.9016	175.5498	173.4803	172.6903	166.9942
217.3568	215.3147	209.0069	194.0424	182.4865	181.1764	180.5352	171.3750
222.2576	219.7203	211.8007	193.0403	187.5779	186.9500	186.4555	174.7803
225.2391	222.2969	213.0576	191.0558	190.4876	190.4052	190.0472	177.1584
226.2781	223.6396	212.8375	188.3588	192.2951	192.7008	192.4658	178.4911
225.4181	222.0027	211.2278	185.1207	193.0282	193.9077	193.7772	178.7700
222.7896	219.7187	208.3628	181.4770	192.9185	194.0865	194.0390	178.0308
218.6670	215.2492	204.4283	177.5751	191.8857	193.3178	193.3319	176.3624
213.5618	210.2730	199.8988	173.7840	190.1106	191.7051	191.7550	173.9158
208.2469	205.1114	195.1659	169.4695	187.5751	189.3130	189.3956	170.9053
204.0046	201.0052	191.5506	166.9223	184.7283	186.4206	186.4788	167.5986
			161.2537	185.2961	185.7803	185.4734	164.2839
			158.7151	184.4040	184.9564	184.5753	161.1565
			157.0104	181.8437	182.3674	181.9758	158.3178
			155.6252	178.8760	179.3556	178.9691	155.8580
			154.4468	175.0005	175.4158	175.0565	153.7995
			153.4451	170.4024	170.7372	170.4240	152.1420
			152.6834	167.2444	167.5259	167.2416	150.8708
			152.0873	160.0144	160.1576	159.9750	149.9378
			151.7285	152.8191	152.8218	152.7467	149.3940

1.1000

216.1006	213.1598	204.5710	186.3934	182.6459	182.2768	182.0765	178.9127
218.0422	214.7803	205.2437	184.9473	185.5127	185.6069	185.5025	180.4750
218.4604	214.9900	204.8231	182.9305	187.3045	187.7948	187.7682	180.9828
217.4778	213.9075	203.4158	180.4997	187.9646	188.7693	188.8017	180.5024
215.3295	211.7503	201.1922	177.7285	187.8985	188.9629	189.0369	179.1518
212.4081	208.8783	198.4239	174.8040	187.1825	188.4421	188.5415	177.0913
209.3316	205.8648	195.5170	171.4532	185.8381	187.2791	187.3984	174.5235
206.7819	203.3640	193.1259	169.3547	184.1340	185.5651	185.6663	171.6754
			164.1910	184.6613	185.2582	184.9485	168.7708
			161.6316	185.4951	186.0441	185.7253	165.9590
			160.0529	184.8974	185.4481	185.0931	163.2737
			158.6792	184.1467	184.9886	184.3082	160.7697
			157.3834	182.4420	182.9745	182.5701	158.4704
			156.1578	179.5942	180.0834	179.6894	156.3990
			155.0586	176.3809	176.8188	176.4458	154.5736
			154.0726	172.5217	172.8939	172.5571	152.9972
			153.2306	168.1544	168.4490	168.1612	151.6808
			152.5542	164.6174	164.8494	164.6013	150.6353
			152.0375	158.6101	158.7267	158.5636	149.8522
			151.7201	152.6662	152.6658	152.5921	149.3793

1.2000

208.3323	205.3369	196.8343	178.9867	181.6825	182.0249	182.0937	180.7911
208.1103	205.0084	196.1391	177.1861	182.6540	183.2695	183.3705	180.0114
207.2884	204.1178	194.9850	175.0995	182.9716	183.8138	183.9363	178.6011
206.2583	203.0295	193.6360	172.6266	182.6326	183.6747	183.8153	176.7345
205.3643	202.0773	192.4562	170.9500	181.9514	183.0496	183.1792	174.5927
			166.4859	182.9612	183.4669	183.2708	172.3435
			164.3718	183.8734	184.3345	184.1381	170.0930
			163.0256	184.8987	185.4065	185.1397	167.8595
			161.8253	184.9361	185.4595	185.1471	165.6496
			160.6189	184.9066	185.4442	185.0902	163.4936
			159.3944	183.8893	184.4215	184.0454	161.4024
			158.1800	182.5992	183.1209	182.7298	159.4022
			156.9966	180.5626	181.0585	180.6675	157.5069
			155.8724	177.6789	178.1310	177.7569	155.7421
			154.8378	174.4340	174.8341	174.4857	154.1382
			153.9146	170.6844	171.0208	170.7096	152.7188
			153.1248	166.5440	166.8070	166.5429	151.5116
			152.4894	162.8570	163.0539	162.8333	150.5412
			152.0106	157.6637	157.7613	157.6132	149.8157
			151.7153	152.5432	152.5403	152.4685	149.3730

1.3000

199.0926	196.3689	188.6337	171.9287	177.4074	178.0253	178.1857	177.0565
199.5490	196.6870	188.4991	170.8032	177.6427	178.3556	178.5219	175.7381
			167.5188	178.9730	179.3522	179.2869	174.2849
			166.1417	180.3666	180.7280	180.6489	172.7676
			165.2319	182.0133	182.4269	182.2788	171.1877
			164.3651	183.0032	183.4482	183.2468	169.5345
			163.4230	183.7079	184.1794	183.9300	167.8200
			162.3987	184.3441	184.8424	184.5464	166.0523
			161.3023	184.1996	184.7099	184.3812	164.2388
			160.1617	183.8139	184.3319	183.9751	162.4042
			158.9975	182.6369	183.1488	182.7781	160.5678
			157.8402	181.1052	181.5998	181.2223	158.7635
			156.7137	178.9408	179.4067	179.3344	157.0209
			155.6452	176.1016	176.5242	176.1702	155.3769
			154.6622	172.9019	173.2729	172.9454	153.8692
			153.7864	169.2825	169.5919	169.3008	152.5292
			153.0384	165.3441	165.5837	165.3374	151.3871
			152.4369	161.6322	161.8048	161.6031	150.4684
			151.9881	156.9978	157.0821	156.9445	149.7858
			151.7108	152.4388	152.4338	152.3637	149.3671

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166.6272	174.7403	174.9813	175.0150	173.5118
166.2729	176.4022	176.6792	176.6647	172.6732
165.8459	178.0554	178.3718	178.3051	171.7234
165.2945	179.5973	179.9530	179.8348	170.6493
164.6148	181.1825	181.5808	181.4085	169.4444
163.8124	182.2185	182.6500	182.4317	168.1052
162.9050	182.9057	183.3646	183.1050	166.6450
161.9107	183.3582	183.8410	183.5429	165.0797
160.8481	183.1463	183.6401	183.3142	163.4290
159.7431	182.5863	183.0845	182.7363	161.7258
158.6185	181.3544	181.8432	181.4843	160.0007
157.5020	179.7144	180.1854	179.8234	158.2931
156.4180	177.5164	177.9576	177.6030	156.6386
155.3924	174.7516	175.1508	174.8146	155.0754
154.4505	171.6318	171.9805	171.6708	153.6406
153.6137	168.1482	168.4377	168.1831	152.3656
152.9039	164.3928	164.6158	164.3838	151.2793
152.3406	160.7295	160.8857	160.6983	150.4057
151.9339	156.4990	156.5744	156.4448	149.7593
151.6956	152.3444	152.3379	152.2693	149.3614

1.5000

165.9180	173.0133	173.2179	173.2383	171.5237
165.6429	174.9859	175.2360	175.2084	170.9938
165.2388	176.8591	177.1547	177.0780	170.2952
164.6977	178.5424	178.8819	178.7564	169.4217
164.0278	180.1024	180.4852	180.3102	168.3756
163.2397	181.1715	181.5888	181.3705	167.1649
162.3510	181.8524	182.2974	182.0405	165.8103
161.3805	182.2016	182.6684	182.3769	164.3362
160.3483	181.9586	182.4357	182.1187	162.7698
159.2793	181.3097	181.7890	181.4529	161.1465
158.1980	180.0654	180.5346	180.1896	159.5003
157.1310	178.3914	178.8414	178.4951	157.8698
156.1028	176.2109	176.6308	176.2927	156.2907
155.1371	173.5364	173.9150	173.5949	154.7995
154.2358	170.5171	170.8464	170.5520	153.4312
153.4775	167.1739	167.4458	167.1850	152.2158
152.8193	163.5920	163.8000	163.5796	151.1808
152.22956	160.0233	160.1658	159.9891	150.3488
151.9159	156.1031	156.1706	156.0472	149.7348
151.6918	152.2568	152.2485	152.1813	149.3559

1.6000

165.2359	171.5326	171.7145	171.7347	170.2837
164.9537	173.6779	173.9099	173.8825	169.8769
164.5564	175.6632	175.9438	175.8679	169.2743
164.0384	177.4098	177.7359	177.6121	168.4786
163.3596	178.9360	179.3045	179.1335	167.4997
162.6321	180.0086	180.4113	180.1985	166.3526
161.7833	180.6752	181.1048	180.8548	165.0610
160.8611	180.9601	181.4094	181.1273	163.6515
159.8847	180.7039	181.1622	180.8560	162.1531
158.8759	180.0162	180.4749	180.1515	160.6003
157.8562	178.7876	179.2355	178.9040	159.0266
156.8490	177.1248	177.5528	177.2209	157.4687
155.8764	174.9941	175.3922	175.0688	155.9612
154.9509	172.4199	172.7781	172.4721	154.5385
154.1237	159.5130	169.8236	169.5425	153.2334
153.3838	166.3109	166.5665	166.3175	152.0748
152.7580	162.8933	163.0879	162.8775	151.0884
152.2503	159.4435	159.5746	159.4065	150.2957
151.9005	155.7732	155.8342	155.7157	149.7115
151.6881	152.1741	152.1642	152.0982	149.3504

1.7000

164.5388	170.2771	170.4439	170.4665	169.2946
164.2855	172.4897	172.7078	172.6827	168.9302
163.9139	174.5073	174.7742	174.7009	168.3665
163.4184	176.2606	176.5724	176.4521	167.6105
162.8076	177.7415	178.0740	177.9284	166.6748
162.0926	178.7973	179.1829	178.9766	165.5767
161.2888	179.4438	179.8550	179.6131	164.3397
160.4131	179.6868	180.1162	179.8439	162.9901
159.4843	179.4271	179.8647	179.5696	161.5568
158.5235	178.7290	179.1660	178.8551	160.0722
157.5520	177.5306	177.9569	177.6385	158.5691
156.5922	175.9034	176.3099	175.9918	157.0819
155.6659	173.8393	174.2166	173.9070	155.6437
154.7943	171.3690	171.7081	171.4152	154.2872
153.9977	168.5797	168.8730	168.6040	153.0433
153.2941	165.5176	165.7582	165.5200	151.9394
152.6993	152.2580	162.4404	162.2389	150.9998
152.2267	158.9409	159.0622	158.9015	150.2448
151.8857	155.4835	155.5388	155.4247	149.6891
151.6846	152.0945	152.0830	152.0182	149.3450

1.8000

163.9050	169.1896	169.3437	169.3670	168.3793
163.6696	171.3999	171.6048	171.5810	168.0331
163.3188	173.3977	173.6505	173.5795	167.4932
162.8478	175.1205	175.4172	175.3005	166.7678
162.2655	176.5463	176.8819	176.7217	165.8703
161.5833	177.5702	177.9378	177.7385	164.8181
160.8161	178.1905	178.5826	178.3492	163.6339
159.9807	178.4026	178.8116	178.5495	162.3431
159.0950	178.1432	178.5598	178.2761	160.9736
158.1794	177.4500	177.8655	177.5671	159.5562
157.2543	176.2895	176.6944	176.3891	158.1222
156.3409	174.7118	175.0974	174.7926	156.7043
155.4599	172.7238	173.0811	172.7847	155.3339
154.6315	170.3594	170.6800	170.3997	154.0421
153.8747	167.6904	167.9672	167.7097	152.8579
153.2065	164.7674	164.9939	164.7658	151.8074
152.6421	161.6616	161.8326	161.6394	150.9136
152.1939	158.4855	158.5979	158.4438	150.1955
151.8711	155.2184	155.2684	155.1583	149.6671
151.6810	152.0167	152.0037	151.9401	149.3396

1.9000

163.2997	168.2173	168.3606	168.3831	167.4921
163.0742	170.3802	170.5731	170.5496	167.1572
162.7382	172.3241	172.5635	172.4944	166.6367
162.2876	173.9923	174.2739	174.1608	165.9394
161.7311	175.3551	175.6740	175.5193	165.0784
161.0801	176.3373	176.6867	176.4946	164.0710
160.3488	176.9270	177.2997	177.0751	162.9386
159.5530	177.1141	177.5025	177.2509	161.7057
158.7102	176.8569	177.2524	176.9802	160.3991
157.8395	176.1775	176.5716	176.2857	159.0479
156.9603	175.0592	175.4430	175.1506	157.6821
156.0929	173.5393	173.9043	173.6127	156.3324
155.2567	171.6329	171.9707	171.6872	155.0289
154.4709	169.3753	169.6781	169.4099	153.8008
153.7534	166.8283	167.0892	166.8428	152.6755
153.1203	164.0438	164.2567	164.0383	151.6776
152.5859	161.0892	161.2493	161.0641	150.8288
152.1518	158.0589	158.1630	158.0151	150.1469
151.8568	154.9681	155.0133	154.9069	149.6454
151.6775	151.9401	151.9255	151.8631	149.3342

2.0000

162.7023	167.3187	167.4528	167.4734	166.6210
162.4848	169.4059	169.5877	169.5641	166.2943
162.1524	171.2749	171.5012	171.4339	165.7913
161.7314	172.8733	173.1400	173.0305	165.1206
161.2004	174.1682	174.4703	174.3213	164.2951
160.5803	175.1022	175.4333	175.2487	163.3314
159.8845	175.6583	176.0116	175.7960	162.2501
159.1282	175.8237	176.1917	175.9505	161.0745
158.3280	175.5698	175.9442	175.6837	159.8301
157.5020	174.9094	175.2823	175.0088	158.5445
156.6686	173.8359	174.1988	173.9192	157.2462
155.8469	172.3786	172.7233	172.4446	155.9642
155.0552	170.5572	170.8739	170.6050	154.7269
154.3117	168.4071	168.6924	168.4360	153.5619
153.6333	165.9830	166.2283	165.9927	152.4948
153.0350	163.3365	163.5362	163.3272	151.5491
152.5302	160.5315	160.6810	160.5035	150.7449
152.1300	157.6498	157.7461	157.6041	150.0989
151.8426	154.7270	154.7674	154.6646	149.6240
151.6739	151.8641	151.8481	151.7868	149.3288

2.1000

162.1344	166.4832	166.6088	166.6269	165.7787
161.9355	168.5053	168.6767	168.6524	165.4708
161.6371	170.3133	170.5275	170.4611	164.9955
161.2353	171.8578	172.1107	172.0040	164.3610
160.7380	173.1042	173.3908	173.2464	163.5794
160.1554	174.0060	174.3203	174.1419	162.6666
159.5001	174.5432	174.8785	174.6707	161.6419
158.7863	174.7013	175.0506	174.8185	160.5273
158.0298	174.4597	174.8131	174.5645	159.3469
157.2474	173.8256	174.1794	173.9166	158.1268
156.4568	172.7983	173.1424	172.8739	156.8937
155.6757	171.4018	171.7285	171.4610	155.6751
154.9218	169.6584	169.9602	169.7002	154.4979
154.2122	167.6030	167.8729	167.6268	153.3881
153.5829	165.2853	165.5171	165.2909	152.3699
152.9886	162.7563	162.9446	162.7436	151.4656
152.5025	160.0766	160.2171	160.0462	150.6944
152.1156	157.3198	157.4094	157.2724	150.0728
151.8368	154.5327	154.5692	154.4694	149.6135
151.6726	151.8023	151.7850	151.7247	149.3265

2.2000

161.6986	165.7317	165.8476	165.8634	165.0397
161.5352	167.7287	167.8892	167.8639	164.7727
161.2743	169.5159	169.7180	169.6521	164.3446
160.9113	171.0451	171.2848	171.1601	163.7624
160.4532	172.2803	172.5530	172.4119	163.0374
159.9094	173.1812	173.4809	173.3071	162.1840
159.2915	173.7255	174.0459	173.8437	161.2200
158.6130	173.8976	174.2317	174.0062	160.1660
157.8888	173.6809	174.0214	173.7782	159.0447
157.1353	173.0795	173.4187	173.1638	157.8807
156.3597	172.0955	172.4258	172.1654	156.6995
155.6096	170.7501	171.0639	170.8045	155.5272
154.8729	159.0666	169.3566	169.1045	154.3898
154.1769	167.0796	167.3390	167.1002	153.3128
153.5383	164.8558	165.0586	164.6389	152.3203
152.9723	162.3858	162.5667	162.3713	151.4348
152.4924	159.7883	159.9231	159.7565	150.6768
152.1101	157.1121	157.1976	157.0638	150.0638
151.8344	154.4110	154.4451	154.3472	149.6099
151.6721	151.7637	151.7457	151.6860	149.3257

2.3000

161.4363	165.0922	165.1971	165.2115	164.4644
161.3054	167.0911	167.2401	167.2146	164.2496
161.0752	168.8829	169.0732	169.0082	163.8758
160.7406	170.4199	170.6477	170.5450	163.3492
160.3081	171.6649	171.9256	171.7876	162.6792
159.7871	172.5808	172.8687	172.6989	161.8794
159.1891	173.1439	173.4529	173.2555	160.9661
158.5277	173.3377	173.6608	173.4406	159.9589
157.8182	173.1481	173.4781	173.2406	158.8796
157.0774	172.5769	172.9062	172.6573	157.7520
156.3227	171.6283	171.9493	171.6950	156.6014
155.5722	170.3216	170.6269	170.3733	155.4541
154.8438	168.6810	168.9634	168.7167	154.3386
154.1550	166.7410	166.9937	166.7599	153.2749
153.5224	164.5468	164.7638	164.5485	152.2941
152.9615	162.1486	162.3248	162.1330	151.4176
152.4856	159.6045	159.7356	159.5719	150.6663
152.1063	156.9802	157.0630	156.9313	150.0581
151.8328	154.3340	154.3665	154.2698	149.6075
151.6717	151.7393	151.7207	151.6614	149.3251

2.4000

161.2909	164.5825	164.6773	164.6917	164.0679
161.1777	166.5968	166.7359	166.7113	163.9028
160.9632	168.4047	168.5855	168.5223	163.5770
160.6424	169.9587	170.1774	170.0772	163.0955
160.2223	171.2209	171.4729	171.3381	162.4670
159.7124	172.1559	172.4355	172.2695	161.7043
159.1244	172.7393	173.0403	172.8470	160.8236
158.4723	172.9538	173.2694	173.0536	159.8441
157.7713	172.7871	173.1101	172.8770	158.7880
157.0381	172.2398	172.5625	172.3180	157.6796
156.2905	171.3174	171.6324	171.3823	156.5447
155.5462	170.0382	170.3380	170.0884	155.4102
154.8234	168.4273	168.7047	168.4617	154.3032
154.1396	166.5190	166.7674	166.5369	153.2502
153.5113	164.3579	164.5712	164.3587	152.2765
152.9538	161.9941	162.1672	161.9777	151.4058
152.4807	159.4850	159.6137	159.4519	150.6589
152.1036	156.8948	156.9759	156.8455	150.0541
151.8317	154.2841	154.3176	154.2198	149.6057
151.6714	151.7235	151.7046	151.6456	149.3247

2.5000

161.1964	164.1964	164.2836	164.2992	163.8202
161.0928	166.2296	166.3616	166.3388	163.6917
160.8872	168.0558	168.2299	168.1690	163.3987
160.5747	169.6277	169.8401	169.7425	162.9458
160.1523	170.9267	171.1527	171.0208	162.3420
159.6596	171.8588	172.1328	171.9698	161.6003
159.0785	172.4590	172.7547	172.5646	160.7372
158.4326	172.6900	173.0006	172.7880	159.7726
157.7374	172.5406	172.8588	172.6289	158.7292
157.0097	172.0107	172.3290	172.0875	157.6315
156.2670	171.1058	171.4178	171.1705	156.5059
155.5272	169.8469	170.1430	169.8961	155.3794
154.8085	168.2564	168.5305	168.2899	154.2793
154.1282	166.3698	166.6153	166.3869	153.2322
153.5029	164.2312	164.4420	164.2313	152.2636
152.9481	161.8906	162.616	161.8737	151.3970
152.4771	159.4051	159.5322	159.3716	150.6534
152.1016	156.8378	156.9178	156.7883	150.0510
151.8308	154.2509	154.2818	154.1864	149.6044
151.6712	151.7130	151.6939	151.6350	149.3244

2.6000

161.1287	163.9139	163.9958	164.0131	163.6687
161.0316	165.9641	166.0911	166.0702	163.5620
160.8320	167.8060	167.9754	167.9166	163.2876
160.5252	169.3925	169.6005	169.5051	162.8506
160.1182	170.6848	170.9267	170.7970	162.2604
159.6206	171.6498	171.9399	171.7592	161.5304
159.0442	172.2625	172.5545	172.3666	160.6776
158.4028	172.5055	172.8126	172.6022	159.7220
157.7118	172.3683	172.6833	172.4555	158.6865
156.9880	171.8507	172.1661	171.9266	157.5960
156.2490	170.9600	171.2681	171.0228	156.4768
155.5126	169.7135	170.0071	169.7620	155.3561
154.7968	168.1373	168.4091	168.1702	154.2610
154.1193	166.2659	166.5094	166.2825	153.2183
153.4964	164.1429	164.3521	164.1427	152.2535
152.9435	161.8185	161.9882	161.8014	151.3900
152.4742	159.3496	159.4756	159.3158	150.6490
152.1000	156.7983	156.8775	156.7486	150.0486
151.8301	154.2279	154.2583	154.1833	149.6034
151.6710	151.7056	151.6864	151.6276	149.3241

2.7000

161.0784	163.7108	163.7890	163.8077	163.5695
160.9857	165.7737	165.8973	165.8779	163.4750
160.7903	167.6272	167.7934	167.7361	163.2111
160.4874	169.2240	169.4290	169.3351	162.7833
160.0842	170.5258	170.7647	170.6366	162.2014
159.5902	171.4998	171.7671	171.6079	161.4788
159.0173	172.1210	172.4105	172.2241	160.6327
158.3792	172.3723	172.6770	172.4681	159.6833
157.6914	172.2437	172.5564	172.3301	158.6534
156.9706	171.7348	172.0480	171.8100	157.5682
156.2344	170.8533	171.1594	170.9155	156.4537
155.5006	169.6165	169.9082	169.6644	155.3373
154.7873	168.0506	168.3207	168.0830	154.2462
154.1119	166.1901	166.4321	166.2063	153.2070
153.4909	164.0785	164.2864	164.0780	152.2451
152.9397	161.7659	161.9346	161.7485	151.3842
152.4718	159.3090	159.4342	159.2750	150.6453
152.0987	156.7695	156.8481	156.7196	150.0465
151.8295	154.2111	154.2411	154.1464	149.6025
151.6709	151.7002	151.6809	151.6222	149.3239

2.8000

161.0394	163.5648	163.6404	163.6601	163.4985
160.9498	165.6362	165.7574	165.7391	163.4111
160.7572	167.4972	167.6611	167.6049	163.1537
160.4572	169.1009	169.3036	169.2109	162.7319
160.0567	170.4087	170.6456	170.5186	162.1554
159.5654	171.3885	171.6539	171.4958	161.4379
158.9950	172.0154	172.3030	172.1178	160.5966
158.3595	172.2723	172.5752	172.3675	159.6518
157.6742	172.1496	172.4606	172.2354	158.6262
156.9558	171.6469	171.9585	171.7215	157.5449
156.2219	170.7720	171.0767	170.8338	156.4343
155.4903	169.5424	169.8327	169.5898	155.3214
154.7790	167.9841	168.2530	168.0161	154.2334
154.1054	166.1319	166.3728	166.1477	153.1971
153.4862	164.0289	164.2359	164.0281	152.2379
152.9364	161.7253	161.8932	161.7077	151.3792
152.4597	159.2776	159.4022	159.2435	150.6421
152.0975	156.7472	156.8253	156.6972	150.0447
151.8289	154.1980	154.2278	154.1333	149.6016
151.6707	151.6960	151.6766	151.6180	149.3237

2.9000

161.0078	163.4584	163.5322	163.5527	163.4439
160.9202	165.5350	165.6545	165.6368	163.3611
160.7297	167.4004	167.5626	167.5072	163.1080
160.4317	169.0079	169.2091	169.1172	162.6902
160.0332	170.3193	170.5547	170.4285	162.1176
159.5440	171.3027	171.5666	171.4093	161.4038
158.9757	171.9331	172.2193	172.0349	160.5661
158.3423	172.1937	172.4952	172.2883	159.6248
157.6590	172.0751	172.3847	172.1604	158.6026
156.9427	171.5768	171.8871	171.6509	157.5247
156.2107	170.7068	171.0103	170.7682	156.4171
155.4810	169.4826	169.7718	169.5297	155.3072
154.7715	167.9302	168.1981	167.9620	154.2220
154.0996	166.0845	166.3245	166.1001	153.1882
153.4818	163.9885	164.1946	163.9874	152.2312
152.9333	161.6921	161.8593	161.6743	151.3745
152.4577	159.2519	159.3759	159.2176	150.6391
152.0963	156.7289	156.8067	156.6789	150.0430
151.8284	154.1873	154.2168	154.1225	149.6009
151.6706	151.6926	151.6731	151.6145	149.3235

3.0000

160.9810	163.3792	163.4517	163.4727	163.3996
160.8948	165.4582	165.5765	165.5594	163.3198
160.7058	167.3257	167.4868	167.4318	163.0696
160.4092	168.9351	169.1351	169.0437	162.6546
160.0124	170.2482	170.4824	170.3568	162.0848
159.5248	171.2334	171.4961	171.3395	161.3739
158.9582	171.8659	172.1509	171.9672	160.5391
158.3266	172.1289	172.4293	172.2230	159.6006
157.6451	172.0130	172.3215	172.0979	158.5814
156.9306	171.5179	171.8272	171.5917	157.5062
156.2004	170.6517	170.9542	170.7127	156.4014
155.4724	169.4318	169.7201	169.4786	155.2941
154.7645	167.8843	168.1513	167.9157	154.2114
154.0941	166.0439	166.2831	166.0593	153.1800
153.4777	163.9537	164.1592	163.9524	152.2250
152.9304	161.6634	161.8301	161.6455	151.3701
152.4658	159.2296	159.3533	159.1953	150.6362
152.0953	156.7131	156.7906	156.6630	150.0414
151.8280	154.1780	154.2074	154.1132	149.6002
151.6705	151.6895	151.6700	151.6115	149.3233

3.1000

160.9372	163.3183	163.3899	163.4112	163.3619
160.8720	165.3979	165.5153	165.4985	163.2840
160.6840	157.2658	167.4259	167.3714	163.0358
160.3387	158.8755	169.0746	168.9836	162.6229
159.9932	170.1891	170.4223	170.2972	162.0553
159.5070	171.1749	171.4367	171.2806	161.3467
158.9419	171.8085	172.0925	171.9093	160.5143
158.3118	172.0728	172.3722	172.1665	159.5783
157.6320	171.9588	172.2664	172.0433	158.5615
156.9191	171.4661	171.7745	171.5396	157.4888
156.1705	170.6030	170.9046	170.6636	156.3866
155.4642	169.3866	169.6741	169.4331	155.2817
154.7378	167.8432	168.1095	167.8744	154.2013
154.0589	166.0075	166.2461	166.0226	153.1720
153.4737	163.9224	164.1273	163.9210	152.2191
152.9276	161.6376	161.8038	161.6195	151.3659
152.4540	159.2095	159.3328	159.1750	150.6335
152.0742	156.6988	156.7760	156.6486	150.6398
151.8275	154.1695	154.1987	154.1047	149.5995
151.6704	151.6868	151.6672	151.6087	149.3232

3.2000

160.9355	163.2698	163.3408	163.3622	163.3283
160.8510	165.3486	165.4652	165.4487	163.2517
160.6538	167.2157	167.3751	167.3208	163.0049
160.3394	168.8247	169.0230	168.9323	162.5937
159.9750	170.1378	170.3702	170.2454	162.0279
159.4900	171.1235	171.3844	171.2287	161.3212
158.9264	171.7573	172.0405	171.8577	160.4908
158.2977	172.0224	172.3210	172.1157	159.5570
157.6194	171.9097	172.2165	171.9939	158.5425
156.9080	171.4189	171.7265	171.4920	157.4722
156.1810	170.5582	170.8590	170.6186	156.3723
155.4562	169.3449	169.6317	169.3912	155.2697
154.7313	167.8052	168.0708	167.8362	154.1915
154.0837	165.9737	166.2117	165.9887	153.1643
153.4699	163.8932	164.0976	163.8917	152.2133
152.9249	151.6135	161.7792	161.5953	151.3618
152.4522	159.1907	159.3136	159.1561	150.6308
152.0732	156.6854	156.7624	156.6351	150.6383
151.8271	154.1616	154.1907	154.0967	149.5988
151.6702	151.6842	151.6645	151.6061	149.3230

3.3000

160.9149	163.2296	163.3000	163.3215	163.2973
160.8309	165.3066	165.4227	165.4062	165.2216
160.6444	167.1720	167.3308	167.2767	162.9759
160.3509	168.7796	168.9772	168.8868	162.5659
159.9575	170.0915	170.3233	170.1988	162.0017
159.4736	171.0766	171.3368	171.1814	161.2967
158.9112	171.7101	171.9926	171.8102	160.4662
158.2839	171.9755	172.2734	172.0685	159.5365
157.6071	171.8638	172.1698	171.9476	158.5241
156.8972	171.3745	171.6813	171.4473	157.4560
156.1717	170.5160	170.8161	170.5761	156.3583
155.4483	169.3055	169.5915	169.3515	155.2579
154.7449	167.7691	168.0341	167.7999	154.1819
154.0787	165.9455	166.1789	165.9563	153.1567
153.4561	163.8654	164.0693	163.8637	152.2076
152.9222	161.5905	161.7558	161.5722	151.3578
152.4605	159.1727	159.2953	159.1381	150.6282
152.0922	156.6726	156.7493	156.6223	150.0368
151.8266	154.1540	154.1829	154.0891	149.5981
151.6701	151.6817	151.6620	151.6036	149.3228

3.4000

160.8952	163.1948	163.2648	163.2863	163.2680
160.8116	165.2694	165.3850	165.3086	163.1929
160.6257	167.1326	167.2908	167.2368	162.9481
160.3329	168.7382	168.9353	168.8451	162.5392
159.9404	170.0486	170.2797	170.1555	161.9763
159.4576	171.0326	171.2921	171.1370	161.2729
158.8964	171.6656	171.9473	171.7053	160.4462
158.2704	171.9310	172.2281	172.0237	159.5163
157.5950	171.8199	172.1252	171.9034	158.5060
156.8865	171.3319	171.6380	171.4044	157.4401
156.1625	170.4754	170.7747	170.5352	156.3445
155.4406	169.2674	169.5528	169.3132	155.2463
154.7386	167.7343	167.9986	167.7648	154.1724
154.0737	165.9104	166.1472	165.9250	153.1493
153.4523	163.8385	164.0419	163.8366	152.2019
152.9195	161.5681	161.7330	161.5497	151.3537
152.4587	159.1552	159.2774	159.1205	150.6256
152.0912	156.6801	156.7366	156.6097	150.0353
151.8262	154.1466	154.1754	154.0817	149.5974
151.6700	151.6792	151.6595	151.6011	149.3226

3.5000

160.8760	163.1637	163.2334	163.2548	163.2398
160.7927	165.2354	165.3506	165.3342	163.1651
160.6073	167.0959	167.2537	167.1998	162.9210
160.3152	168.6993	168.8958	168.8058	162.5131
159.9235	170.0078	170.2383	170.1144	161.9514
159.4418	170.9904	171.2494	171.0945	161.2495
158.8818	171.6227	171.9038	171.7220	160.4245
158.2570	171.8879	172.1844	171.9803	159.4965
157.5830	171.7773	172.0819	171.8605	158.4882
156.8759	171.2905	171.5959	171.3627	157.4243
156.1534	170.4357	170.7344	170.4953	156.3309
155.4329	169.2302	169.5149	169.2758	155.2348
154.7323	167.7001	167.9639	167.7305	154.1630
154.0687	165.8799	166.1161	165.8943	153.1418
153.4586	163.8120	164.0149	163.8100	152.1963
152.9169	161.5462	161.7106	161.5276	151.3498
152.4570	159.1380	159.2599	159.1032	150.6230
152.0903	156.6478	156.7241	156.5974	150.0338
151.8257	154.1393	154.1679	154.0743	149.5968
151.6699	151.6768	151.6570	151.5987	149.3225

3.6000

160.8571	163.1350	163.2043	163.2258	163.2123
160.7741	165.2035	165.3183	165.3020	163.1379
160.5891	167.0611	167.2184	167.1646	162.8944
160.2977	168.6619	168.8580	168.7680	162.4874
159.9069	169.9684	170.1984	170.0746	161.9268
159.4261	170.9495	171.2078	171.0533	161.2263
158.8672	171.5808	171.8613	171.6799	160.4030
158.2438	171.8458	172.1416	171.9378	159.4768
157.5710	171.7355	172.0395	171.8185	158.4705
156.8654	171.2498	171.5545	171.3217	157.4086
156.1443	170.3967	170.6947	170.4560	156.3174
155.4253	169.1936	169.4776	169.2389	155.2234
154.7260	167.6664	167.9296	167.6966	154.1537
154.0638	165.8497	166.0854	165.8639	153.1344
153.4549	163.7859	163.9883	163.7838	152.1907
152.9143	161.5245	161.6885	161.5058	151.3458
152.4553	159.1210	159.2426	159.0861	150.6204
152.0893	156.6357	156.7117	156.5852	150.0324
151.8253	154.1321	154.1606	154.0671	149.5961
151.6698	151.6745	151.6546	151.5963	149.3223

3.7000

160.8385	163.1078	163.1769	163.1983	163.1853
160.7557	165.1729	165.2874	165.2710	163.1111
160.5711	167.0274	167.1843	167.1306	162.8681
160.2803	168.6256	168.8211	168.7314	162.4619
159.8903	169.9299	170.1593	170.0357	161.9025
159.4105	170.9094	171.1671	171.0128	161.2034
158.8527	171.5397	171.8195	171.6384	160.3816
158.2305	171.8043	172.0594	171.8960	159.4572
157.5591	171.6943	171.9975	171.7769	158.4528
156.8549	171.2095	171.5135	171.2812	157.3931
156.1352	170.3581	170.6554	170.4171	156.3039
155.4176	169.1572	169.4407	169.2023	155.2120
154.7198	167.6330	167.8596	167.6630	154.1443
154.0589	165.8198	166.0550	165.8339	153.1270
153.4312	163.7600	163.9619	163.7577	152.1851
152.9116	161.5029	161.6666	161.4841	151.3418
152.4536	159.1041	159.2254	159.0691	150.6178
152.0883	156.6237	156.6994	156.5731	150.5309
151.8248	154.1250	154.1533	154.0599	149.5955
151.6697	151.6721	151.6522	151.5940	149.3221

3.8000

160.8200	163.0817	163.1506	163.1718	163.1585
160.7374	165.1432	165.2574	165.2410	163.0845
160.5532	166.9945	167.1510	167.0974	162.8419
160.2630	168.5899	168.7850	168.6953	162.4366
159.8738	169.8920	170.1208	169.9975	161.8783
159.3950	170.8697	171.1269	170.9728	161.1805
158.8383	171.4989	171.7781	171.5973	160.3603
158.2174	171.7631	172.0575	171.8545	159.4377
157.5473	171.6534	171.9559	171.7357	158.4352
156.8445	171.1695	171.4728	171.2409	157.3775
156.1262	170.3197	170.6164	170.3785	156.2904
155.4100	169.1211	169.4040	169.1660	155.2007
154.7136	167.5998	167.8618	167.6296	154.1350
154.0540	165.7901	166.0247	165.8039	153.1197
153.4475	163.7342	163.9357	163.7317	152.1796
152.9090	161.4814	161.6447	161.4625	151.3379
152.4518	159.0873	159.2082	159.0522	150.6152
152.0573	156.6117	156.6872	156.5610	150.0294
151.8244	154.1178	154.1460	154.0527	149.5948
151.6696	151.6698	151.6498	151.5916	149.3220

3.9000

160.8015	163.0562	163.1249	163.1460	163.1318
160.7192	165.1141	165.2279	165.2116	163.0580
160.5354	166.9621	167.1183	167.0646	162.8159
160.2458	168.5547	168.7493	168.6598	162.4114
159.8573	169.8544	170.0828	169.0595	161.8541
159.3795	170.8304	171.0870	170.9332	161.1577
158.8239	171.4585	171.7370	171.5565	160.3390
158.2042	171.7222	172.0160	171.8132	159.4182
157.5355	171.6126	171.9146	171.6947	158.4177
156.8340	171.1297	171.4323	171.2008	157.3620
156.1172	170.2814	170.5775	170.3400	156.2770
155.4024	169.0852	169.3673	169.1298	155.1893
154.7073	167.5667	167.8281	167.5963	154.1257
154.0491	165.7604	165.9945	165.7741	153.1123
153.4437	163.7685	163.9095	163.7059	152.1740
152.9064	161.4600	161.6229	161.4410	151.3339
152.4501	159.0705	159.1911	159.0353	150.6126
152.0563	156.5997	156.6750	156.5490	150.0279
151.8240	154.1107	154.1388	154.0456	149.5941
151.6595	151.6674	151.6474	151.5892	149.3218

4.0000

160.7831	163.0312	163.0996	163.1207	163.1053
160.7010	165.0854	165.1989	165.1825	163.0316
160.5176	166.9301	167.0858	167.0322	162.7900
160.2286	168.5197	168.7139	168.6245	162.3862
159.8409	169.8171	170.0449	169.9219	161.8300
159.3540	170.7913	171.0473	170.8937	161.1349
158.8095	171.4182	171.6961	171.5159	160.3178
158.1910	171.6814	171.9745	171.7721	159.3987
157.5236	171.5721	171.8733	171.6538	158.4001
156.8236	171.0899	171.3920	171.1668	157.3465
156.1082	170.2433	170.5387	170.3016	156.2635
155.3948	169.0493	169.3308	169.0936	155.1780
154.7011	167.5337	167.7945	167.5630	154.1164
154.0441	165.7308	165.9643	165.7443	153.1049
153.4400	163.6828	163.8833	163.6880	152.1684
152.9037	161.4387	161.6011	161.4195	151.3299
152.4484	159.0538	159.1741	159.0185	150.6101
152.0854	156.5877	156.6628	156.5370	150.0265
151.8235	154.1036	154.1315	154.0384	149.5935
151.6594	151.6651	151.6450	151.5869	149.3216

A NEW MAXIMUM COMPUTATION TIME MUST BE PLACED AFTER THE VARIABLE DUMP IF THIS PROBLEM IS TO BE CONTINUED.

## CARD DUMP OUTPUT

0.00000+000	0.00000+000	0.00000+000	0.00000+000	0.00000+000	0.00000+000	0.00000+000
0.00000+000	1.00913+000	1.00885+000	0.00000+000	0.00000+000	0.00000+000	0.00000+000
3.82680-001	0.00000+000	1.89083+003	1.57932+003	3.67357+006	1.40548+001	
2.69383+001	2.55540+006	2.55704+006	0.00000+000	6.11555+001	6.11975+001	
1.50026+002	8.24444+001	1.67684+002	2.04400+004	2.74017+004	8.35419+001	
2.94912+003	7.07665+004	4.50651+005	1.15207+004	3.02105+005	4.07389+004	
1.05936+005	1.40753+005	1.54159+005	4.07389+004	1.05936+005	2.88637+005	
1.00818+004	4.07389+004	1.05936+005	2.63314+003	7.05841+004	4.49378+005	
3.68640+004	7.33956+004	1.05936+005	4.60800+003	1.38240+004	7.33956+004	
1.05936+005	1.57989+004	6.55116+003	7.33956+004	1.05936+005	3.64089+003	
4.55111+003	3.64270+004	2.88339+005	1.00917+000	1.00892+000	0.00000+000	
0.00000+000	0.00000+000	5.22500+001	3.67581+003	1.89309+003	1.58256+003	
5.01578+006	1.91900+001	3.67808+001	3.48873+006	3.49074+006	0.00000+000	
6.11485+001	6.11875+001	1.50610+002	3.49024+001	1.67656+002	8.80844+005	
2.74022+004	3.60000+001	2.94912+003	8.78113+004	4.49912+005	1.15388+004	
3.02105+005	5.06371+004	1.05936+005	1.40753+005	1.54159+005	5.06371+004	
1.05936+005	2.88637+005	1.01080+004	5.06371+004	1.05936+005	2.63314+003	
8.74879+004	4.48159+005	3.68640+004	9.00370+004	1.05936+005	4.60800+003	
1.38240+004	9.00370+004	1.05936+005	1.57989+004	7.37419+003	9.00370+004	
1.05936+005	3.64089+003	4.55111+003	3.96734+004	1.14419+005	1.00923+000	
1.00901+000	0.00000+000	0.00000+000	0.00000+000	6.49450+001	4.13761+003	
1.89606+003	1.58667+003	6.23445+006	2.38525+001	4.57173+001	4.33583+006	
4.33796+006	0.00000+000	6.11398+001	6.11748+001	1.51330+002	3.49024+001	
1.67622+002	8.80876+005	2.74026+004	3.60000+001	2.94912+003	1.02620+005	
4.49014+005	1.15609+004	3.02105+005	5.92886+004	1.05936+005	1.40753+005	
1.54159+005	5.92886+004	1.05936+005	2.88637+005	1.01392+004	5.92886+004	
1.05936+005	2.63314+003	1.02094+005	4.46715+005	3.68640+004	1.04025+005	
1.05936+005	4.60800+003	1.38240+004	1.04025+005	1.05936+005	1.57989+004	
8.17364+003	1.04025+005	1.05936+005	3.64089+003	4.55111+003	4.13340+004	
1.03201+005	1.00929+000	1.00912+000	0.00000+000	0.00000+000	0.00000+000	
7.60410-001	4.58618+003	1.89969+003	1.59158+003	7.29961+006	2.79277+001	
5.35281+001	5.07583+006	5.07785+006	0.00000+000	6.11295+001	6.11596+001	
1.52168+002	3.49024+001	1.67580+002	8.80904+005	2.74030+004	3.60000+001	
2.94912+003	1.14772+005	4.47979+005	1.15864+004	3.02105+005	6.64797+004	
1.05936+005	1.40753+005	1.54159+005	6.64797+004	1.05936+005	2.88637+005	
1.01748+004	6.64797+004	1.05936+005	2.63314+003	1.14045+005	4.45083+005	
3.68640+004	1.15079+005	1.05936+005	4.60800+003	1.38240+004	1.15079+005	
1.05936+005	1.57989+004	8.95129+003	1.15079+005	1.05936+005	3.64089+003	
4.55111+003	4.17386+004	9.42175+004	1.00937+000	1.00924+000	0.00000+000	
0.00000+000	0.00000+000	8.52640+001	5.02251+003	1.90389+003	1.59716+003	
8.18498+006	3.13151+001	6.00206+001	5.69046+006	5.69214+006	6.00000+000	
6.11178+001	6.11423+001	1.53310+002	3.49024+001	1.67533+002	8.80927+005	
2.74033+004	3.60000+001	2.34912+003	1.24033+005	4.46835+005	1.16148+004	
3.02105+005	7.20343+004	1.05936+005	1.40753+005	1.54159+005	7.20343+004	
1.05936+005	2.88637+005	1.02138+004	7.20343+004	1.05936+005	2.63314+003	
1.23063+005	4.43303+005	3.68640+004	1.23423+005	1.05936+005	4.60800+003	
1.38240+004	1.23423+005	1.05936+005	1.57989+004	9.55162+003	1.23423+005	
1.05936+005	3.64089+003	4.55111+003	4.19319+004	8.82739+004	1.00946+000	
1.00938+000	0.00000+000	0.00000+000	0.00000+000	9.23880+001	5.35935+003	
1.90855+003	1.60329+003	8.86886+006	3.39315+001	6.50354+001	6.16469+006	
6.16582+006	0.00000+000	6.11051+001	6.11234+001	1.54116+002	3.49024+001	
1.67481+002	8.80943+005	2.74036+004	3.60000+001	2.94912+003	1.30172+005	
4.45607+005	1.16454+004	3.02105+005	7.58150+004	1.05936+005	1.40753+005	
1.54159+005	7.58150+004	1.05936+005	2.88637+005	1.02555+004	7.58150+004	
1.05936+005	2.63314+003	1.28953+005	4.41420+005	3.68640+004	1.28117+005	
1.05936+005	4.60800+003	1.38240+004	1.28217+005	1.05936+005	1.57989+004	
1.02847+004	1.28117+005	1.05936+005	3.64089+003	4.55111+003	4.04204+004	
8.19778+004	1.00956+000	1.00953+000	0.00000+000	0.00000+000	0.00000+000	
9.72370+001	5.77067+003	1.31358+003	1.60984+003	9.33434+006	3.57124+001	
6.84488+001	6.48685+006	6.48729+006	0.00000+000	6.17916+001	6.11032+001	

1.55177+002 3.49024-001 1.67425-002 8.80953-005 2.74037-004 3.60000-001  
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 $-1.83749 \times 10^7 - 1.12250 \times 10^8 - 6.87806 \times 10^7 - 1.71269 \times 10^7 - 1.71448 \times 10^7 - 1.71249 \times 10^7$   
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 $1.51587 \times 10^2$   $1.49285 \times 10^2$   $1.30000 \times 10^2$   $1.30000 \times 10^2$   $1.30000 \times 10^2$   $1.51738 \times 10^2$   
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 $1.89478 \times 10^2$   $1.60357 \times 10^2$   $1.66930 \times 10^2$   $1.67086 \times 10^2$   $1.67032 \times 10^2$   $1.62646 \times 10^2$   
 $1.98886 \times 10^2$   $1.96052 \times 10^2$   $1.87953 \times 10^2$   $1.60599 \times 10^2$   $1.65085 \times 10^2$   $1.65199 \times 10^2$   
 $1.65183 \times 10^2$   $1.62945 \times 10^2$   $1.96018 \times 10^2$   $1.93436 \times 10^2$   $1.86102 \times 10^2$   $1.60737 \times 10^2$   
 $1.63031 \times 10^2$   $1.63100 \times 10^2$   $1.63121 \times 10^2$   $1.63079 \times 10^2$   
 $-4.53227 \times 10^5$   $5.74693 \times 10^3$   $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   
 $0.00000 \times 1000$   $0.00000 \times 1000$   $1.47456 \times 10^3$   $-2.62735 \times 10^5$   $7.03767 \times 10^4$   $0.00000 \times 1000$   
 $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   $1.51052 \times 10^5$   
 $-2.53392 \times 10^5$   $1.44319 \times 10^5$   $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   
 $0.00000 \times 1000$   $0.00000 \times 1000$   $7.70793 \times 10^4$   $-2.55274 \times 10^5$   $1.31657 \times 10^3$   $0.00000 \times 1000$   
 $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   $5.01917 \times 10^3$   
 $-4.52727 \times 10^5$   $0.00000 \times 1000$   
 $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   
 $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$   $0.00000 \times 1000$







```

1,44319+005 0.00000+000 0.00000+000 0.00000+000 0.00000+000 0.00000+000
0.00000+000 7.70793+004-2.55809+005 1,31657+003 0.00000+000 0.00000+000
0.00000+000 0.00000+000 0.00000+000 0.00000+000 5,55422+003-4.07422+005
-4.36947+005 5.95238+003 0.00000+000 0.00000+000 0.00000+000 0.00000+000
0.00000+000 0.00000+000 1.47456+003-2.62941+005 7.03767+004 0.00000+000
0.00000+000 0.00000+000 0.00000+000 0.00000+000 0.00000+000 1.51052+005
-2.53392+005 1.44319+005 0.00000+000 0.00000+000 0.00000+000 0.00000+000
0.00000+000 0.00000+000 7.70793+004-2.55550+005 1.31657+003 0.00000+000
0.00000+000 0.00000+000 0.00000+000 0.00000+000 0.00000+000 5.29548+003
-4.28145+005 7.03767+004 0.00000+000 0.00000+000 0.00000+000 0.00000+000
0.00000+000 0.00000+000 1.51052+005-2.53392+005 1.44319+005 0.00000+000
0.00000+000 0.00000+000 0.00000+000 0.00000+000 0.00000+000 7.70793+004
-2.55818+005 1.31657+003 0.00000+000 0.00000+000 0.00000+000 0.00000+000
0.00000+000 0.00000+000 5.56296+003-4.06756+005 4.36698+005 5.95565+003
0.00000+000 0.00000+000 0.00000+000 0.00000+000 0.00000+000 0.00000+000
1.47456+003-2.62944+005 7.03767+004 0.00000+000 0.00000+000 0.00000+000 0.00000+000
0.00000+000 0.00000+000 0.00000+000 1.51052+005-2.53392+005 1.44319+005
0.00000+000 0.00000+000 0.00000+000 0.00000+000 0.00000+000 0.00000+000
7.70793+004-2.55553+005 1.31657+003 0.00000+000 0.00000+000 0.00000+000 0.00000+000
0.00000+000 0.00000+000 0.00000+000 5.29830+003-4.27908+005 7.03767+004
0.00000+000 0.00000+000 0.00000+000 0.00000+000 0.00000+000 0.00000+000
1.51052+005-2.53392+005 1.44319+005 0.00000+000 0.00000+000 0.00000+000 0.00000+000
0.00000+000 0.00000+000 0.00000+000 7.70793+004-2.55582+005 1.31657+003
0.00000+000 0.00000+000 0.00000+000 0.00000+000 0.00000+000 0.00000+000
5.56656+003-4.06483+005

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## APPENDIX B

FORTRAN Listing of TRANTEMP CodePROGRAM TRANTEMP

THIS IS THE MAIN SUBROUTINE.

THIS CODE HAS BEEN NAMED TRANTEMP (TRANSIENT TEMPERATURE) AND IS USED TO DETERMINE THE TIME-DEPENDENT TEMPERATURE MAP OF A HYDRAULIC RABBIT ASSEMBLY. IT HAS BEEN ASSIGNED THE ARGONNE NATIONAL LABORATORY IDENTIFICATION NUMBER RE418X.

PROGRAM TRANTEMP	TRAN	1
THIS IS THE MAIN SUBROUTINE.	TRAN	2
THIS CODE HAS BEEN NAMED TRANTEMP (TRANSIENT TEMPERATURE) AND IS	TRAN	3
USED TO DETERMINE THE TIME-DEPENDENT TEMPERATURE MAP OF A	TRAN	4
HYDRAULIC RABBIT ASSEMBLY. IT HAS BEEN ASSIGNED THE ARGONNE	TRAN	5
NATIONAL LABORATORY IDENTIFICATION NUMBER RE418X.	TRAN	6
X	TRAN	7
X	TRAN	8
X	TRAN	9
X	TRAN	10
X	TRAN	11
DIMENSION A(8,8),A1(50),A2(50),A3(50),A4(50),A5(50),A6(50),A7(50),	TRAN	12
XAB(50),A9(50),A10(50),A11(50),A12(50),A13(50),A14(50),A15(50),	TRAN	13
XA16(50),A17(50),A18(50),	TRAN	14
XB1(50),B2(50),B3(50),B4(50),B5(50),B6(50),B7(50),B8(50),B9(50),	TRAN	15
XB10(50),B11(50),B12(50),B13(50),B14(50),B15(50),	TRAN	16
XCP4(50),CP8(50),	TRAN	17
XD(8),DIS4(50),DIS8(50),	TRAN	18
XF(8,50),FRAC8(50),	TRAN	19
XG(8,8,50),	TRAN	20
XHEAT(50),HL3(50),HL5(50),HL7(50),	TRAN	21
XIFRAC8(50),	TRAN	22
XQAL(50),QALWPG(50),QH20(50),QH204(50),QH208(50),	TRAN	23
XR(8),REMAN8(50),RH04(50),RH08(50),	TRAN	24
XSTORE(50),	TRAN	25
XT(8,50),TFLW(50),THEAT(50),TITCFLOW(50),TPOSN(50),	TRAN	26
XVEQUIV(50),VINTMD(50),VOL1(50),VOL3(50),VSTORE(50),	TRAN	27
XYFLOW(50),YHEAT(50),YTITCFLOW(50),YPOSN(50)	TRAN	28
TYPE LOGICAL DEBUG	TRAN	29
COMMON/1/DEBUG/2/TIME,TPCSN,YPOSN,PRABT/3/MPOSV/4/TFLW,YFLW,	TRAN	30
XMFLOW,GPRIMARY,G1,G2,G3,GZERO/5/R/8/RNUDE,RLNGLTH,RHO4,RHRVS4,	TRAN	31
XRMOVE,	TRAN	32
XFACTOR,TRVRS4/9/T/10/JJ,K1,K2,KK1,KKK2/11/HEAT,THEAT,YHEAT,QH20,	TRAN	33
XQALWPG,QMAXW,QMAXM/12/MHEAT/14/CONDAL,RHOAL,CP4,CP8,RH08,HL5,	TRAN	34
XHL7,D1,D2,D3,DELR1,DELR2,DELR5,DELR6,R3TRM,RBTRM2,TMPIN4,	TRAN	35
XTPIN8/15/IRABT,IRABT2,MRVRS/16/VOL3,VOLND3,STORE,DTAU,VOLND1,	TRAN	36
XRRTNOD,RBTEND,RNDEND,RHRVS8,TRVRS8	TRAN	37
COMMON/17/MITCFLOW,TITCFLOW,YITCFLOW	TRAN	38
1 FORMAT(6E12.5)	TRAN	39
2 FORMAT(6I12)	TRAN	40
3 FORMAT(36X,7F12.4)	TRAN	41
4 FORMAT(1X,F11.4,9F12.4)	TRAN	42
5 FORMAT(1X,E11.4,9E12.4)	TRAN	43
6 FORMAT(1X,F11.4,9E12.4)	TRAN	44
7 FORMAT(1X,I11,9I12)	TRAN	45
8 FORMAT(/)	TRAN	46
9 FORMAT(1H1)	TRAN	47
10 FORMAT(34H COOLANT WATER EXPANSION TOO LARGE)	TRAN	48
11 FORMAT(1X,E11.4,F12.4,2I12)	TRAN	49
12 FORMAT(1X,E11.4,E12.4,I12,E12.4)	TRAN	50
13 FORMAT(1X,F11.5,5F12.5)	TRAN	51
14 FORMAT(10H NEW MAXIMUM COMPUTATION TIME MUST BE PLACED AFTER THTRAN	TRAN	52
XE VARIABLE DUMP IF THIS PROBLEM IS TO BE CONTINUED.)	TRAN	53
15 FORMAT(L12,5I12)	TRAN	54
16 FORMAT(52X,17H INPUT INFORMATION/)	TRAN	55
17 FORMAT(53X,15H COMPUTED OUTPUT/)	TRAN	56
18 FORMAT(10H CARD 6***,3X,11HTOTAL AXIAL,2X,13HAXIAL SECTION,	TRAN	57
X3X,13HAXIAL SECTION,3X,26HTOTAL NUMBER OF NORMALIZED,3X,	TRAN	58
X15HTOTAL NUMBER OF,3X,15HTOTAL NUMBER OF/14X,8HSECTIONS,5X,	TRAN	59
X10HCONTAINING,4X,14HCONTAINING TOP,6X,20HHEAT GENERATION RATE,6X, TRAN	TRAN	60



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40 FORMAT(9X,6F12.4/) TRAN 121
41 FORMAT(6X,1HZ) TRAN 122
42 FORMAT(1X,1H(,I2,1H),F7.4,42X,1HX,11X,1HX,11X,1HX,11X,1HX)TRAN 123
43 FORMAT(1X,1H(,I2,1H),F7.4,6X,1HX,11X,1HX,11X,1HX,11X,1HX,1HX)TRAN 124
  X11X,1HX,11X,1HX,11X,1HX) TRAN 125
44 FORMAT(12H CARDS 16***,34X,27HRABBIT POSITION VERSUS TIME// TRAN 126
  X33X,14HTIME (SECONDS),15X,24HRABBIT POSITION (INCHES)) TRAN 127
45 FORMAT(1H1,12HMAIN PROGRAM//) TRAN 128
46 FORMAT(1X,I5) TRAN 129
47 FORMAT(9A8) TRAN 130
48 FORMAT(24X,9A8) TRAN 131
49 FORMAT(12H CARDS 15***,28X,40HNORMALIZED PRIMARY FLOW RATE VERSUS TRAN 132
  XTIME//33X,14HTIME (SECONDS),18X,20HNORMALIZED FLOW RATE) TRAN 133
C TRAN 134
C TRAN 135
C NEW PROBLEM BEGINS HERE TRAN 136
C TRAN 137
C TRAN 138
100 CONTINUE TRAN 139
LSTEDY=0 TRAN 140
MPRINT=0 TRAN 141
MRVRS=0 TRAN 142
TIME=0, TRAN 143
PRINT 9 TRAN 144
READ 2, MPASS TRAN 145
IF(EOF,60)1850,110 TRAN 146
110 IF(MPASS-1)111,1802,1792 TRAN 147
111 CONTINUE TRAN 148
PRINT 16 TRAN 149
DO 112 I=1,4 TRAN 150
READ 47, T1,T2,T3,T4,T5,T6,T7,T8,T9 TRAN 151
112 PRINT 48, T1,T2,T3,T4,T5,T6,T7,T8,T9 TRAN 152
PRINT 8 $ PRINT 8 TRAN 153
READ 2, JJ,K1,K2,MHEAT,MFLOW,MPOSN TRAN 154
READ 15, DEBUG,MOPT,MSTEDY,MEND,NPRINT,MITCFLOW TRAN 155
READ 1, (R(I),I=2,8) TRAN 156
READ 1, ZTUBE,RLNGTH,PRABT,DTAU,TDEBUG,TFINAL TRAN 157
READ 1, QMAXW,QMAXM,GZERO,IPRIMARY TRAN 158
READ 1, TSTART,TMPIN4,TMF1N8,CONDAL,RHOAL,CPAL TRAN 159
READ 1, (HEAT(J),J=1,JJ) TRAN 160
READ 1, (THEAT(I),YHEAT(I),I=1,MHEAT) TRAN 161
READ 1, (TFLW(I),YFLW(I),I=1,MFLOW) TRAN 162
READ 1, (TITCFLOW(I),YITCFLOW(I),I=1,MITCFLOW) TRAN 163
READ 1, (TPOSN(I),YPCSN(I),I=1,MPOSN) TRAN 164
IF(MOPT)120,120,150 TRAN 165
120 DO 140 J=1,JJ TRAN 166
DO 130 K=1,8 TRAN 167
130 T(K,J)=TSTART TRAN 168
140 CONTINUE TRAN 169
GO TO 170 TRAN 170
150 DO 160 J=1,JJ TRAN 171
I=JJ-J+1 TRAN 172
160 READ 1, (T(K,I),K=1,8) TRAN 173
170 CONTINUE TRAN 174
PRINT 18 TRAN 175
PRINT 19, JJ,K1,K2,MHEAT,MFLOW,MPOSN TRAN 176
PRINT 8 TRAN 177
PRINT 20 TRAN 178
PRINT 21, DEBUG,MOPT,MSTEDY,MEND,NPRINT,MITCFLOW TRAN 179
PRINT 8 TRAN 180

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PRINT 8	TRAN 181
PRINT 22	TRAN 182
PRINT 23, 0.,,(R(I),I=2,8)	TRAN 183
PRINT 8	TRAN 184
PRINT 8	TRAN 185
PRINT 24	TRAN 186
PRINT 25, ZTUBE,RLNGTH,PRABT,DTAU,TDEBUG,TFINAL	TRAN 187
PRINT 8	TRAN 188
PRINT 8	TRAN 189
PRINT 26	TRAN 190
PRINT 27, QMAXH,QMAXM,GZERO,GPRIMARY	TRAN 191
PRINT 8	TRAN 192
PRINT 8	TRAN 193
PRINT 28	TRAN 194
PRINT 29, TSTART,TMPIN4,TMPIN8,CONDAL,RHOAL,CPAL	TRAN 195
PRINT 8	TRAN 196
PRINT 8	TRAN 197
PRINT 30	TRAN 198
PRINT 31, (J,HEAT(J),J=1,JJ)	TRAN 199
PRINT 8	TRAN 200
PRINT 8	TRAN 201
PRINT 32	TRAN 202
PRINT 33, (THEAT(I),YHEAT(I),I=1,MHEAT)	TRAN 203
PRINT 8	TRAN 204
PRINT 8	TRAN 205
PRINT 34	TRAN 206
PRINT 33, (TFLLOW(I),YFLLOW(I),I=1,MFLLOW)	TRAN 207
PRINT 8	TRAN 208
PRINT 8	TRAN 209
PRINT 49	TRAN 210
PRINT 33, (TITCFLOW(I),YITCFLOW(I),I=1,MITCFLOW)	TRAN 211
PRINT 8	TRAN 212
PRINT 8	TRAN 213
PRINT 44	TRAN 214
PRINT 33, (TPOSN(I),YPOSN(I),I=1,MPOSN)	TRAN 215
PRINT 9	TRAN 216
PRINT 17	TRAN 217
PRINT 38	TRAN 218
PRINT 39	TRAN 219
PRINT 40, 0.,,(R(I),I=2,8)	TRAN 220
PRINT 41	TRAN 221
KK1=K1+1	TRAN 222
KK2=K2+1	TRAN 223
AXIAL=ZTUBE*(1.-(.5/JJ))	TRAN 224
DO 171 J=KKK2,JJ	TRAN 225
K=JJ+KKK2-J	TRAN 226
PRINT 42, K,AXIAL	TRAN 227
171 AXIAL=AXIAL-(ZTUBE/JJ)	TRAN 228
DO 172 J=K1,K2	TRAN 229
K=K2+K1-J	TRAN 230
PRINT 43, K,AXIAL	TRAN 231
172 AXIAL=AXIAL-(ZTUBE/JJ)	TRAN 232
DO 173 J=1,KK1	TRAN 233
K=KK1+1-J	TRAN 234
PRINT 42, K,AXIAL	TRAN 235
173 AXIAL=AXIAL-(ZTUBE/JJ)	TRAN 236
PRINT 9	TRAN 237
PRINT 35	TRAN 238
PRINT 4, 0,	TRAN 239
DO 180 J=KKK2,JJ	TRAN 240

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K=JJ+KKK2-J
180 PRINT 3, (T(I,K),I=4,8)          TRAN 241
DO 190 J=K1,K2                      TRAN 242
K=K2+K1-J                          TRAN 243
190 PRINT 4, (T(I,K),I=1,8)          TRAN 244
DO 200 J=1,KK1                      TRAN 245
K=KK1+1-J                          TRAN 246
200 PRINT 3, (T(I,K),I=4,8)          TRAN 247
PRINT 8                            TRAN 248
TRVRS4=T(4,1)                      TRAN 249
TRVRS8=T(8,1)                      TRAN 250
PRINT 8                            TRAN 251
DO 210 L=2,8                      TRAN 252
210 R(L)=R(L)/12.                  TRAN 253
DELR1=R(2)                        TRAN 254
DELR2=DELR1                      TRAN 255
DELR5=R(6)-R(5)                  TRAN 256
DELR6=DELR5                      TRAN 257
D1=2.*R(5)                        TRAN 258
D2=2.*(R(5)-R(3))                TRAN 259
D3=2.*(R(8)-R(7))                TRAN 260
TDEBUG=TDEBUG/3600.                TRAN 261
DTAU=DTAU/3600.                   TRAN 262
RLNGTH=RLNGTH/12.                 TRAN 263
ZTUBE=ZTUBE/12.                   TRAN 264
PRABT=PRABT/12.                   TRAN 265
RNODE=ZTUBE/JJ                     TRAN 266
VOLND3=3.1415927*(R(8)**2-R(7)**2)*RNODE
RBTNOD=PRABT/RNODE                TRAN 267
IRABT=RBTNOD                      TRAN 268
RBTRM=RBTNOD-IRABT                TRAN 269
IF(RBTRM-.5)220,220,230
220 K1=IRABT*1                    TRAN 270
GO TO 240                         TRAN 271
230 K1=IRABT+2                    TRAN 272
240 CONTINUE                       TRAN 273
      RRTEND=PRABT+RLNGTH          TRAN 274
      RNDEND=RBTRM/RNODE          TRAN 275
      IRABT2=RNDEND              TRAN 276
      RBTRM2=RNDEND-IRABT2        TRAN 277
      IF(RBTRM2-.5)250,250,260
250 K2=IRABT2                      TRAN 278
      GO TO 270                  TRAN 279
260 K2=IRABT2+1                    TRAN 280
270 CONTINUE                       TRAN 281
      G1=GZERO                     TRAN 282
      G3=GPRIMARY                  TRAN 283
      RHOIN4=DENSE(TMPIN4)          TRAN 284
      RHOIN8=DENSE(TMPIN8)          TRAN 285
C
C
C
C   ENTRY POINT FOR PROBLEM CONTINUATION IN THE NEXT TIME INTERVAL
C
C
C
300 CALL FLOW
  IF(TIME-TDEBUG)304,303,303          TRAN 293
303 DEBUG=0                          TRAN 294
304 IF(TIME)100,305,305            TRAN 295
                                         TRAN 296
                                         TRAN 297
                                         TRAN 298
                                         TRAN 299
                                         TRAN 300

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305 IF(DEBUG) GO TO 320          TRAN 301
PRINT 45                          TRAN 302
PRINT 46, 305                     TRAN 303
PRINT 5, DELR1,DELR2,DELR5,DELR6,D1,D2,D3,DTAU,RLNGTH,ZTUBE
PRINT 5, TPRINT,R(3),R(5),G1,G2,G3   TRAN 304
PRINT 8                           TRAN 305
PRINT 8                           TRAN 306
PRINT 8                           TRAN 307
320 CONTINUE                      TRAN 308
C
  IF(K2-JJ)321,321,322           TRAN 309
  322 K2=JJ                        TRAN 310
  IF(K1-JJ)321,321,323           TRAN 311
  323 K1=JJ+1                     TRAN 312
  321 CONTINUEF                   TRAN 313
  IF(KKK2-JJ)324,324,325         TRAN 314
  325 KKK2=JJ+1                  TRAN 315
  IF(KK1-JJ)324,324,326         TRAN 316
  326 KK1=JJ                      TRAN 317
  324 CONTINUE                     TRAN 318
C
  RABBIT-FREE SECTION            TRAN 319
  DO 330 J=1,KK1                 TRAN 320
  CALL WATER(T(4,J),D1,G1,HL5(J),RH04(J),CP4(J))    TRAN 321
  330 CONTINUE                     TRAN 322
  DO 340 J=KKK2,JJ                TRAN 323
  CALL WATER(T(4,J),D1,G1,HL5(J),RH04(J),CP4(J))    TRAN 324
  340 CONTINUE                     TRAN 325
C
  RABBIT SECTION ONLY            TRAN 326
  DO 350 J=K1,K2                 TRAN 327
  CALL WATER(T(4,J),D2,G2,HL5(J),RH04(J),CP4(J))    TRAN 328
  HL3(J)=HL5(J)                  TRAN 329
  350 CONTINUE                     TRAN 330
  IF(DEBUG) GO TO 400             TRAN 331
  PRINT 46, 350                  TRAN 332
  DO 370 J=1,KK1                 TRAN 333
  370 PRINT 6, T(4,J),D1,G1,HL5(J),RH04(J),CP4(J)    TRAN 334
  DO 380 J=K1,K2                 TRAN 335
  380 PRINT 6, T(4,J),D2,G2,HL5(J),RH04(J),CP4(J)    TRAN 336
  DO 390 J=KKK2,JJ                TRAN 337
  390 PRINT 6, T(4,J),D1,G1,HL5(J),RH04(J),CP4(J)    TRAN 338
  PRINT 8                         TRAN 339
  PRINT 8                         TRAN 340
  400 CONTINUE                     TRAN 341
C
  OUTER WATER                     TRAN 342
  DO 410 J=1,JJ                  TRAN 343
  CALL WATER(T(8,J),D3,G3,HL7(J),RH08(J),CP8(J))    TRAN 344
  410 CONTINUE                     TRAN 345
  IF(DEBUG) GO TO 440             TRAN 346
  PRINT 46, 430                  TRAN 347
  DO 430 J=1,JJ                  TRAN 348
  430 PRINT 6, T(8,J),D3,G3,HL7(J),RH08(J),CP8(J)    TRAN 349
  PRINT 8                         TRAN 350
  PRINT 8                         TRAN 351
  440 CONTINUE                     TRAN 352
  CALL QHEAT                      TRAN 353
  IF(TIME)100,405,405             TRAN 354
  405 DO 450 J=1,JJ                TRAN 355
  QH204(J)=1551.0774*RH04(J)*QH20(J)    TRAN 356
  QH208(J)=1551.0774*RH08(J)*QH20(J)    TRAN 357
  TRAN 358
  TRAN 359
  TRAN 360

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450 QAL(J)=1551.0774*RHOAL*QALWPG(J) TRAN 361
  IF(DEBUG) GO TO 480 TRAN 362
  PRINT 46, 470 TRAN 363
  DO 470 J=1,JJ TRAN 364
470 PRINT 5, QH204(J),QH208(J),QAL(J) TRAN 365
  PRINT 8 TRAN 366
  PRINT 8 TRAN 367
480 CONTINUE TRAN 368
C
  IF(LSTEDY)4480,4480,483 TRAN 369
4480 IF(MSTEDY)482,482,481 TRAN 370
  CALL STEADY TRAN 371
  IF(MEND)100*100,481 TRAN 372
481 LSTEDY=1 TRAN 373
  PRINT 9 TRAN 374
  GO TO 300 TRAN 375
483 CONTINUE TRAN 376
C
  RABBIT=FREE SECTION TRAN 377
  DO 490 J=1,KK1 TRAN 378
A1(J)=2./R(5)**2 TRAN 379
A2(J)=QH204(J)/(HL5(J)*R(5)) TRAN 380
A3(J)=(RH04(J)*CP4(J))/(HL5(J)*R(5)*DTAU) TRAN 381
A4(J)=(8.+HL5(J)*R(5))/(CONDAL*DELR5*(4.*R(5)+DELR5)) TRAN 382
A5(J)=(4.*2.*R(5)+DELR5)/((DELR5**2)*(4.*R(5)*DELR5)) TRAN 383
A6(J)=QAL(J)/CONDAL TRAN 384
A7(J)=(RHOAL*CPAL)/(CONDAL*DTAU) TRAN 385
A8(J)=(2.*R(6)-DELR5)/(2.*R(6)*DELR6**2) TRAN 386
A9(J)=(2.*R(6)+DELR6)/(2.*R(6)*DELR6**2) TRAN 387
A10(J)=A6(J) TRAN 388
A11(J)=A7(J) TRAN 389
A12(J)=(4.*2.*R(7)-DELR6)/((DELR6**2)*(4.*R(7)-DELR6)) TRAN 390
A13(J)=(8.*HL7(J)*R(7))/(CONDAL*DELR6*(4.*R(7)-DELR6)) TRAN 391
A14(J)=A6(J) TRAN 392
A15(J)=A7(J) TRAN 393
A16(J)=2./R(8)**2-R(7)**2 TRAN 394
A17(J)=QH208(J)/(HL7(J)*R(7)) TRAN 395
490 A18(J)=(RH08(J)*CP8(J))/(HL7(J)*R(7)*DTAU) TRAN 396
  DO 500 J=KK2,JJ TRAN 397
A1(J)=2./R(5)**2 TRAN 398
A2(J)=QH204(J)/(HL5(J)*R(5)) TRAN 399
A3(J)=(RH04(J)*CP4(J))/(HL5(J)*R(5)*DTAU) TRAN 400
A4(J)=(8.+HL5(J)*R(5))/(CONDAL*DELR5*(4.*R(5)+DELR5)) TRAN 401
A5(J)=(4.*2.*R(5)+DELR5)/((DELR5**2)*(4.*R(5)*DELR5)) TRAN 402
A6(J)=QAL(J)/CONDAL TRAN 403
A7(J)=(RHOAL*CPAL)/(CONDAL*DTAU) TRAN 404
A8(J)=(2.*R(6)-DELR5)/(2.*R(6)*DELR6**2) TRAN 405
A9(J)=(2.*R(6)+DELR6)/(2.*R(6)*DELR6**2) TRAN 406
A10(J)=A6(J) TRAN 407
A11(J)=A7(J) TRAN 408
A12(J)=(4.*2.*R(7)-DELR6)/((DELR6**2)*(4.*R(7)-DELR6)) TRAN 409
A13(J)=(8.*HL7(J)*R(7))/(CONDAL*DELR6*(4.*R(7)-DELR6)) TRAN 410
A14(J)=A6(J) TRAN 411
A15(J)=A7(J) TRAN 412
A16(J)=2./R(8)**2-R(7)**2 TRAN 413
A17(J)=QH208(J)/(HL7(J)*R(7)) TRAN 414
500 A18(J)=(RH08(J)*CP8(J))/(HL7(J)*R(7)*DTAU) TRAN 415
  IF(RBTRM,.5)520,520,510 TRAN 416
510 A2(KK1)=A2(KK1)*(1./QH204(KK1))*((1.-RBTRM)*QH204(KK1) TRAN 417
  X*RBTRM*((R(5)**2)-(R(3)**2))/(R(5)**2)*QH204(KK1) TRAN 418
  X*RBTRM*((R(3)**2)/(R(5)**2))*QAL(KK1)) TRAN 419
                                         TRAN 420

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```

520 CONTINUE
  IF(RBTRM2=.5)530,530,540
530 A2(KKK2)=A2(KKK2)*(1./QH204(KKK2))*((1.-RBTRM2)*QH204(KKK2)
  X+RBTRM2*((R(5)**2)-(R(3)**2))/(R(5)**2))*QH204(KKK2)
  X+RBTRM2*((R(3)**2)/(R(5)**2))*QAL(KKK2)
540 CONTINUE
  IF(DEBUG) GO TO 580
  PRINT 46, 560
  DO 560 J=1,KK1
560 PRINT 5, A1(J),A2(J),A3(J),A4(J),A5(J),A6(J),A7(J),A8(J),A9(J),
  XA10(J),A11(J),A12(J),A13(J),A14(J),A15(J),A16(J),A17(J),A18(J)
  DO 570 J=KKK2,JJ
570 PRINT 5, A1(J),A2(J),A3(J),A4(J),A5(J),A6(J),A7(J),A8(J),A9(J),
  XA10(J),A11(J),A12(J),A13(J),A14(J),A15(J),A16(J),A17(J),A18(J)
  PRINT 8
  PRINT 8
580 CONTINUE
C   C   RABBIT-FREE SECTION
  DO 590 J=1,KK1
F(1,J)=-.5*A1(J)*(T(5,J)-T(4,J))-A2(J)-A3(J)*T(4,J)
F(2,J)=-.5*A4(J)*(T(4,J)-T(5,J)),-.5*A5(J)*(T(6,J)-T(5,J))
X-A6(J)=A7(J)*T(5,J)
F(3,J)=-.5*A8(J)*(T(5,J)-T(6,J)),-.5*A9(J)*(T(7,J)-T(6,J))
XA10(J)=A11(J)*T(6,J)
F(4,J)=-.5*A12(J)*(T(6,J)-T(7,J)),-.5*A13(J)*(T(8,J)-T(7,J))
XA14(J)=A15(J)*T(7,J)
590 F(5,J)=-.5*A16(J)*(T(7,J)-T(8,J))-A17(J)-A18(J)*T(8,J)
  DO 600 J=KKK2,JJ
F(1,J)=-.5*A1(J)*(T(5,J)-T(4,J))-A2(J)-A3(J)*T(4,J)
F(2,J)=-.5*A4(J)*(T(4,J)-T(5,J)),-.5*A5(J)*(T(6,J)-T(5,J))
XA6(J)=A7(J)*T(5,J)
F(3,J)=-.5*A8(J)*(T(5,J)-T(6,J)),-.5*A9(J)*(T(7,J)-T(6,J))
XA10(J)=A11(J)*T(6,J)
F(4,J)=-.5*A12(J)*(T(6,J)-T(7,J)),-.5*A13(J)*(T(8,J)-T(7,J))
XA14(J)=A15(J)*T(7,J)
600 F(5,J)=-.5*A16(J)*(T(7,J)-T(8,J))-A17(J)-A18(J)*T(8,J)
  IF(DEBUG) GO TO 640
  PRINT 46, 620
  DO 620 J=1,KK1
620 PRINT 5, F(1,J),F(2,J),F(3,J),F(4,J),F(5,J)
  DO 630 J=KKK2,JJ
630 PRINT 5, F(1,J),F(2,J),F(3,J),F(4,J),F(5,J)
  PRINT 8
  PRINT 8
640 CONTINUE
C   C   RABBIT-FREE SECTION
  DO 650 J=1,KK1
G(1,1,J)=-.5*A1(J)-A3(J)
G(1,2,J)=-.5*A1(J)
G(2,1,J)=-.5*A4(J)
G(2,2,J)=-.5*A4(J)-.5*A5(J)-A7(J)
G(2,3,J)=-.5*A5(J)
G(3,2,J)=-.5*A8(J)
G(3,3,J)=-.5*A8(J)-.5*A9(J)-A11(J)
G(3,4,J)=-.5*A9(J)
G(4,3,J)=-.5*A12(J)
G(4,4,J)=-.5*A12(J)-.5*A13(J)-A15(J)
G(4,5,J)=-.5*A13(J)

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G(5,4,J)=.5*A16(J)          TRAN 481
650 G(5,5,J)=-.5*A16(J)-A18(J) - TRAN 482
DO 660 J=KKK2,JJ              TRAN 483
G(1,1,J)=-.5*A1(J)-A3(J)    TRAN 484
G(1,2,J)=.5*A1(J)           TRAN 485
G(2,1,J)=.5*A4(J)           TRAN 486
G(2,2,J)=-.5*A4(J)-.5*A5(J)=A7(J) TRAN 487
G(2,3,J)=.5*A5(J)           TRAN 488
G(3,2,J)=.5*A8(J)           TRAN 489
G(3,3,J)=-.5*A8(J)-.5*A9(J)=A11(J) TRAN 490
G(3,4,J)=.5*A9(J)           TRAN 491
G(4,3,J)=.5*A12(J)          TRAN 492
G(4,4,J)=-.5*A12(J)-.5*A13(J)=A15(J) TRAN 493
G(4,5,J)=.5*A13(J)          TRAN 494
G(5,4,J)=.5*A16(J)          TRAN 495
660 G(5,5,J)=-.5*A16(J)-A18(J) TRAN 496
IF(DEBUG) GO TO 700          TRAN 497
PRINT 46, 680                TRAN 498
DO 680 J=1,KK1                TRAN 499
680 PRINT 5, G(1,1,J),G(1,2,J),G(2,1,J),G(2,2,J),G(2,3,J),G(3,2,J),
   XG(3,3,J),G(3,4,J),G(4,3,J),G(4,4,J),G(4,5,J),G(5,4,J),G(5,5,J) TRAN 500
   DO 690 J=KKK2,JJ              TRAN 501
690 PRINT 5, G(1,1,J),G(1,2,J),G(2,1,J),G(2,2,J),G(2,3,J),G(3,2,J),
   XG(3,3,J),G(3,4,J),G(4,3,J),G(4,4,J),G(4,5,J),G(5,4,J),G(5,5,J) TRAN 502
   PRINT 8                      TRAN 503
   PRINT 8                      TRAN 504
700 CONTINUE                   TRAN 505
C
C      RABBIT SECTION ONLY
DO 710 J=1,K2                TRAN 506
A4(J)=(8.*HL5(J)*R(5))/(CONDAL*DELR5*(4.*R(5)+DELR5)) TRAN 507
A5(J)=(4.*(2.*R(5)+DELR5))/((DELR5**2)*(4.*R(5)+DELR5)) TRAN 508
A6(J)=QAL(J)/CONDAL          TRAN 509
A7(J)=(RHOAL*CPAL)/(CONDAL*DTAU) TRAN 510
A8(J)=(2.*R(6)+DELR6)/(2.*H(6)*DELR6**2) TRAN 511
A9(J)=(2.*R(6)+DELR6)/(2.*H(6)*DELR6**2) TRAN 512
A10(J)=A6(J)                 TRAN 513
A11(J)=A7(J)                 TRAN 514
A12(J)=(4.*(2.*R(7)-DELR6))/((DELR6**2)*(4.*R(7)-DELR6)) TRAN 515
A13(J)=(8.*HL7(J)*R(7))/(CONDAL*DELR6*(4.*R(7)-DELR6)) TRAN 516
A14(J)=A6(J)                 TRAN 517
A15(J)=A7(J)                 TRAN 518
A16(J)=2./((R(8)**2-R(7)**2) TRAN 519
A17(J)=OH208(J)/(HL7(J)*R(7)) TRAN 520
A18(J)=(RH08(J)*CP8(J))/(HL7(J)*R(7)*DTAU) TRAN 521
B1(J)=4./((DELR1**2)          TRAN 522
B2(J)=QAL(J)/CONDAL          TRAN 523
B3(J)=(RHOAL*CPAL)/(CONDAL*DTAU) TRAN 524
B4(J)=(2.*R(2)-DELR1)/(2.*H(2)*DELR1**2) TRAN 525
B5(J)=(2.*R(2)+DELR2)/(2.*H(2)*DELR1**2) TRAN 526
B6(J)=B2(J)                  TRAN 527
B7(J)=B3(J)                  TRAN 528
B8(J)=(4.*(2.*R(3)-DELR2))/((DELR2**2)*(4.*R(3)-DELR2)) TRAN 529
B9(J)=(8.*HL3(J)*R(3))/((CONDAL*DELR2)*(4.*R(3)-DELR2)) TRAN 530
B10(J)=R2(J)                 TRAN 531
B11(J)=R3(J)                 TRAN 532
B12(J)=(2.*HL3(J)*R(3))/((H(5)**2-H(3)**2)*(HL3(J)*R(3)
   X+HL5(J)*R(5)))          TRAN 533
B13(J)=(2.*HL5(J)*R(5))/((H(5)**2-R(3)**2)*(HL3(J)*R(3)
   X+HL5(J)*R(5)))          TRAN 534

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B14(J)=QH204(J)/(HL3(J)*R(3)+HL5(J)*R(5))
710 B15(J)=(RH04(J)*CP4(J))/(DTAU*(HL3(J)*R(3)+HL5(J)*R(5)))
IF(RBTRM=.5)720,720,730
720 B2(K1)=B2(K1)*(1./QAL(K1))*(RBTRM*QH204(K1)+(1.-RBTRM)*QAL(K1))
B6(K1)=R2(K1)
B10(K1)=B2(K1)
730 CONTINUE
IF(RBTRM2=.5)750,750,740
740 B2(K2)=B2(K2)*(1./QAL(K2))*((1.-RBTRM2)*QH204(K2)+RBTRM2*QAL(K2))
B6(K2)=R2(K2)
B10(K2)=B2(K2)
750 CONTINUE
IF(DEBUG) GO TO 780
PRINT 46, 770
DO 770 J=K1,K2
770 PRINT 5, B1(J),B2(J),B3(J),B4(J),B5(J),B6(J),B7(J),B8(J),B9(J),
XB10(J),R11(J),B12(J),B13(J),B14(J),B15(J)
PRINT 8
PRINT 8
780 CONTINUE
C
C      RABBIT SECTION ONLY
DO 790 J=K1,K2
F(1,J)=-.5*B1(J)*(T(2,J)-T(1,J))-B2(J)*B3(J)*T(1,J)
F(2,J)=-.5*B4(J)*(T(1,J)-T(2,J))-,.5*B5(J)*(T(3,J)-T(2,J))
X-B6(J)=B7(J)*T(2,J)
F(3,J)=-.5*B8(J)*(T(2,J)-T(3,J))-,.5*B9(J)*(T(4,J)-T(3,J))
X-B10(J)=B11(J)*T(3,J)
F(4,J)=-.5*B12(J)*(T(3,J)-T(4,J))-,.5*B13(J)*(T(5,J)-T(4,J))
X-R14(J)=B15(J)*T(4,J)
F(5,J)=-.5*A4(J)*(T(4,J)-T(5,J))-,.5*A5(J)*(T(6,J)-T(5,J))
X-A6(J)=A7(J)*T(5,J)
F(6,J)=-.5*A8(J)*(T(5,J)-T(6,J))-,.5*A9(J)*(T(7,J)-T(6,J))
X-A10(J)=A11(J)*T(6,J)
F(7,J)=-.5*A12(J)*(T(6,J)-T(7,J))-,.5*A13(J)*(T(8,J)-T(7,J))
X-A14(J)=A15(J)*T(7,J)
790 F(8,J)=-.5*A16(J)*(T(7,J)-T(8,J))-A17(J)-A18(J)*T(8,J)
IF(DEBUG) GO TO 820
PRINT 46, 810
DO 810 J=K1,K2
810 PRINT 5, F(1,J),F(2,J),F(3,J),F(4,J),F(5,J),F(6,J),F(7,J),F(8,J)
PRINT 8
PRINT 8
820 CONTINUE
C
C      RABBIT SECTION ONLY
DO 830 J=K1,K2
G(1,1,J)=-.5*B1(J)-B3(J)
G(1,2,J)=-.5*B1(J)
G(2,1,J)=-.5*B4(J)
G(2,2,J)=-.5*B4(J)-.5*B5(J)-B7(J)
G(2,3,J)=-.5*B5(J)
G(3,2,J)=-.5*B8(J)
G(3,3,J)=-.5*B8(J)-.5*B9(J)-B11(J)
G(3,4,J)=-.5*B9(J)
G(4,3,J)=-.5*B12(J)
G(4,4,J)=-.5*B12(J)-.5*B13(J)-B15(J)
G(4,5,J)=-.5*B13(J)
G(5,4,J)=-.5*A4(J)
G(5,5,J)=-.5*A4(J)-.5*A5(J)-A7(J)

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G(5,6,J)=.5*A5(J)          TRAN 601
G(6,5,J)=.5*A8(J)          TRAN 602
G(6,6,J)=-.5*A8(J)-.5*A9(J)=A11(J)  TRAN 603
G(6,7,J)=.5*A9(J)          TRAN 604
G(7,6,J)=.5*A12(J)          TRAN 605
G(7,7,J)=-.5*A12(J)-.5*A13(J)=A15(J)  TRAN 606
G(7,8,J)=.5*A13(J)          TRAN 607
G(8,7,J)=.5*A16(J)          TRAN 608
830 G(8,8,J)=-.5*A16(J)-A18(J)  TRAN 609
IF(DEBUG) GO TO 860          TRAN 610
PRINT 46, 850                TRAN 611
DO 850 J=K1,K2                TRAN 612
850 PRINT 5, G(1,1,J),G(1,2,J),G(2,1,J),G(2,2,J),G(2,3,J),G(3,2,J),
    XG(3,3,J),G(3,4,J),G(4,3,J),G(4,4,J),G(4,5,J),G(5,4,J),G(5,5,J),
    XG(5,6,J),G(6,5,J),G(6,6,J),G(6,7,J),G(7,6,J),G(7,7,J),G(7,8,J),
    XG(8,7,J),G(8,8,J)          TRAN 613
    PRINT 8                      TRAN 614
    PRINT 8                      TRAN 615
860 CONTINUE                  TRAN 616
C
    KK1=K1-1                   TRAN 617
    KKK2=K2+1                   TRAN 618
C
C   BOTTOM WATER SECTION      TRAN 619
DO 950 J=1,KK1                TRAN 620
A(1,1)=G(1,1,J)              TRAN 621
A(1,2)=G(1,2,J)              TRAN 622
DO 880 I=2,4                  TRAN 623
III=I-1                     TRAN 624
DO 870 III=I,3                TRAN 625
A(I,III)=0(I,III,J)          TRAN 626
870 III=III+1                TRAN 627
880 CONTINUE                  TRAN 628
A(5,4)=G(5,4,J)              TRAN 629
A(5,5)=G(5,5,J)              TRAN 630
DO 890 N=1,5                  TRAN 631
890 D(N)=F(N,J)              TRAN 632
IF(DEBUG) GO TO 910          TRAN 633
PRINT 46, 890                TRAN 634
PRINT 5, A(1,1),A(1,2),D(1)  TRAN 635
PRINT 5, A(2,1),A(2,2),A(2,3),D(2)  TRAN 636
PRINT 5, A(3,2),A(3,3),A(3,4),D(3)  TRAN 637
PRINT 5, A(4,3),A(4,4),A(4,5),D(4)  TRAN 638
PRINT 5, A(5,4),A(5,5),D(5)        TRAN 639
910 CONTINUE                  TRAN 640
CALL GAUSS1(A,5,D)          TRAN 641
DO 920 N=1,5                  TRAN 642
NN=N+3                       TRAN 643
920 T(NN,J)=D(N)              TRAN 644
IF(DEBUG) GO TO 940          TRAN 645
PRINT 46, 920                TRAN 646
PRINT 3, (T(LMN,J),LMN=4,8)  TRAN 647
PRINT 8                      TRAN 648
PRINT 8                      TRAN 649
940 CONTINUE                  TRAN 650
950 CONTINUE                  TRAN 651
C
C   RABBIT SECTION            TRAN 652
DO 1040 J=K1,K2                TRAN 653
A(1,1)=G(1,1,J)              TRAN 654

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A(1,2)=G(1,2,J)
DO 970 I=2,7
III=I-1
DO 960 II=1,3
A(I,III)=G(I,III,J)
960 III=III+1
970 CONTINUE
A(8,7)=G(8,7,J)
A(8,8)=G(8,8,J)
DO 980 N=1,8
980 D(N)=F(N,J)
IF(DEBUG) GO TO 1000
PRINT 46, 980
PRINT 5, A(1,1),A(1,2),D(1)
PRINT 5, A(2,1),A(2,2),A(2,3),D(2)
PRINT 5, A(3,2),A(3,3),A(3,4),D(3)
PRINT 5, A(4,3),A(4,4),A(4,5),D(4)
PRINT 5, A(5,4),A(5,5),A(5,6),D(5)
PRINT 5, A(6,5),A(6,6),A(6,7),D(6)
PRINT 5, A(7,6),A(7,7),A(7,8),D(7)
PRINT 5, A(8,7),A(8,8),D(8)
1000 CONTINUE
CALL GAUSS1(A,B,D)
DO 1010 N=1,8
1010 T(N,J)=D(N)
IF(DEBUG) GO TO 1030
PRINT 46, 1010
PRINT 4, (T(LMN,J),LMN=1,8)
PRINT 8
PRINT 8
1030 CONTINUE
1040 CONTINUE
C
C      UPPER WATER SECTION
DO 1130 J=KKK2,JJ
A(1,1)=G(1,1,J)
A(1,2)=G(1,2,J)
DO 1060 I=2,4
III=I-1
DO 1050 II=1,3
A(I,III)=G(I,III,J)
1050 III=III+1
1060 CONTINUE
A(5,4)=G(5,4,J)
A(5,5)=G(5,5,J)
DO 1070 N=1,5
1070 D(N)=F(N,J)
IF(DEBUG) GO TO 1090
PRINT 46, 1070
PRINT 5, A(1,1),A(1,2),D(1)
PRINT 5, A(2,1),A(2,2),A(2,3),D(2)
PRINT 5, A(3,2),A(3,3),A(3,4),D(3)
PRINT 5, A(4,3),A(4,4),A(4,5),D(4)
PRINT 5, A(5,4),A(5,5),D(5)
1090 CONTINUE
CALL GAUSS1(A,5,D)
DO 1100 N=1,5
NN=N+3
1100 T(NN,J)=D(N)
IF(DEBUG) GO TO 1120

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PRINT 46, 1100
PRINT 3, (T(LMN,J),LMN=4,8)
PRINT 8
PRINT 8
1120 CONTINUE
1130 CONTINUE
C
1131 IF(MPRINT-NPRINT)1169,1132,1132
1132 CONTINUE
TPRINT=(TIME+DTAU)*3600.
PRINT 4, TPRINT
DO 1140 J=KKK2,JJ
K=JJ+KKK2-J
1140 PRINT 3, (T(I,K),I=4,8)
DO 1150 J=K1,K2
K=K2+K1-J
1150 PRINT 4, (T(I,K),I=1,8)
DO 1160 J=1,KK1
K=KK1+1-J
1160 PRINT 3, (T(I,K),I=4,8)
PRINT 8
PRINT 8
IF(TIME)1162,1162,1161
1161 MPRINT=0
GO TO 1169
1162 MPRINT=1
C
C
C
1169 CONTINUE
TIME=TIME+DTAU
CALL FLOW
IF(TIME)100,1170,1170
1170 MPRINT=MPRINT+1
IF(G1)1175,1171,1171
1171 IF(TRVRS4=T(4,1))1173,1172,1172
1173 TRVRS4=T(4,1)
RHRVS4=DENSE(TRVRS4)
1172 IF(TRVRS8=T(8,1))1174,1175,1175
1174 TRVRS8=T(8,1)
RHRVS8=DENSE(TRVRS8)
1175 IF(DEBUG) GO TO 1180
PRINT 46, 1175
PRINT 5, VOLND3
1180 CONTINUE
DO 1190 J=1,JJ
VINTMD(J)=VOLND3*RHO8(J)
RHO8(J)=DENSE(T(8,J))
1190 VOL3(J)=VINTMD(J)/RHO8(J)
IF(DEBUG) GO TO 1205
PRINT 46, 1190
PRINT 5, (VINTMD(J),J=1,JJ)
PRINT 8
PRINT 5, (RHO8(J),J=1,JJ)
PRINT 8
PRINT 5, (VOL3(J),J=1,JJ)
PRINT 8
1205 CONTINUE
DO 1210 J=1,JJ
      TRAN 721
      TRAN 722
      TRAN 723
      TRAN 724
      TRAN 725
      TRAN 726
      TRAN 727
      TRAN 728
      TRAN 729
      TRAN 730
      TRAN 731
      TRAN 732
      TRAN 733
      TRAN 734
      TRAN 735
      TRAN 736
      TRAN 737
      TRAN 738
      TRAN 739
      TRAN 740
      TRAN 741
      TRAN 742
      TRAN 743
      TRAN 744
      TRAN 745
      TRAN 746
      TRAN 747
      TRAN 748
      TRAN 749
      TRAN 750
      TRAN 751
      TRAN 752
      TRAN 753
      TRAN 754
      TRAN 755
      TRAN 756
      TRAN 757
      TRAN 758
      TRAN 759
      TRAN 760
      TRAN 761
      TRAN 762
      TRAN 763
      TRAN 764
      TRAN 765
      TRAN 766
      TRAN 767
      TRAN 768
      TRAN 769
      TRAN 770
      TRAN 771
      TRAN 772
      TRAN 773
      TRAN 774
      TRAN 775
      TRAN 776
      TRAN 777
      TRAN 778
      TRAN 779
      TRAN 780

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1210 STORE(J)=T(8,J)
  IF(DEBUG) GO TO 1220
  PRINT 46, 1210
  PRINT 4, (STORE(J),J=1,JJ)
  PRINT 8
1220 IF(G1)1221,1224,1224
1221 CALL REVRSE
  IF(MRVR$)1223,1223,100
1223 IF(TIME)100,1224,1224
1224 IF(G3)1225,1222,1222
1225 CALL PREVRSE
  IF(MRVR$)1226,1226,100
1226 IF(TIME)100,1411,1411
1222 VOLEXS=0.
  L=1
  M=0
  DO 1280 J=2,JJ
  K=JJ-J+1
  VOLEXS=VOLEXS+VOL3(K+1)-VOLND3
  IF(VOLND3-VOLEXS)1230,1240,1240
1230 T(8,K)=STORE(K+L)
  VOLEXS=VOLEXS-VOLND3
  M=M+1
  L=L+1
  GO TO 1250
1240 CONTINUE
  T(8,K)=(VOLEXS*RHO8(K+L)*STORE(K+L)+(VOLND3-VOLEXS)*RHO8(K+M)
  *STORE(K+M))/(VOLEXS*RHO8(K+L)+(VOLND3-VOLEXS)*RHO8(K+M))
1250 CONTINUE
  IF(DEBUG) GO TO 1270
  PRINT 46, 1250
  PRINT 11, VOLEXS,T(8,K),M,L
1270 CONTINUE
1280 CONTINUE
C
  DO 1290 J=1,JJ
1290 RHO8(J)=DENSE(T(8,J))
  IF(DEBUG) GO TO 1310
  PRINT 46, 1290
  PRINT 8
  PRINT 4, (RHO8(J),J=1,JJ)
  PRINT 8
1310 CONTINUE
C
  DO 1320 J=1,JJ
1320 STORE(J)=T(8,J)
  IF(DEBUG) GO TO 1340
  PRINT 46, 1320
  PRINT 4, (STORE(J),J=1,JJ)
  PRINT 8
1340 CONTINUE
  VOLREP=(G3*3,1415927*(R(8)**2-R(7)**2)*DTAU)/RHOINB
  ADVNCE=VOLREP/VOLND3
  I=ADVNCE-I
  REMAIN=ADVNCE-I
  IF(DEBUG) GO TO 1360
  PRINT 46, 1340
  PRINT 8
  PRINT 12, VOLREP,ADVNCE,I,REMAIN   *

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1360 CONTINUE          TRAN 841
DO 1370 J=1,I          TRAN 842
K=JJ-J+1              TRAN 843
1370 T(8,K)=TMPIN8    TRAN 844
INTERM=J+I             TRAN 845
T(8,INTERM)=(REMAIN*TMPIN8*RHOIN8+(1.-REMAIN)*STORE(JJ)  TRAN 846
X*RHO8(JJ))/(REMAIN*RHOIN8+(1.-REMAIN)*RHO8(JJ))      TRAN 847
IJKLMN=I+2            TRAN 848
DO 1380 J=IJKLMN,JJ   TRAN 849
K=JJ-J+1              TRAN 850
1380 T(8,K)=(REMAIN*STORE(K+I+1)*RHO8(K+I+1)+(1.-REMAIN)*STORE(K+I)  TRAN 851
X*RHO8(K+I))/(REMAIN*RHO8(K+I+1)+(1.-REMAIN)*RHO8(K+I))  TRAN 852
C                      TRAN 853
DO 1390 J=1,JJ          TRAN 854
1390 RHO8(J)=DENSE(T(8,J))  TRAN 855
C                      TRAN 856
IF(DEBUG) GO TO 1410  TRAN 857
PRINT 46, 1390        TRAN 858
PRINT 8               TRAN 859
PRINT 4, (T(8,J),J=1,JJ)  TRAN 860
PRINT 8               TRAN 861
PRINT 4, (RHO8(J),J=1,JJ)  TRAN 862
PRINT 8               TRAN 863
1410 CONTINUE          TRAN 864
C                      TRAN 865
C                      TRAN 866
C                      TRAN 867
1411 IF(G1)1780,1412,1412  TRAN 868
1412 CONTINUE          TRAN 869
C                      TRAN 870
C                      TRAN 871
C                      TRAN 872
VOLND1=3.1415927*(R(5)**2)*RNODE          TRAN 873
FACTOR=(R(5)**2-R(3)**2)/(R(5)**2)          TRAN 874
DO 1420 J=1,IRABT          TRAN 875
VOL1(J)=VOLND1          TRAN 876
I15=IRART*1              TRAN 877
VOL1(I15)=RBTRM*VOLND1+(1.-RBTRM)*VOLND1*FACTOR  TRAN 878
I16=I15*1                TRAN 879
DO 1430 J=I16,K2          TRAN 880
VOL1(J)=FACTOR*VOLND1          TRAN 881
I17=K2*1                TRAN 882
VOL1(I17)=RBTRM2*FACTOR*VOLND1+(1.-RBTRM2)*VOLND1  TRAN 883
I18=I17*1                TRAN 884
DO 1440 J=I18,JJ          TRAN 885
VOL1(J)=VOLND1          TRAN 886
IF(DEBUG) GO TO 1460  TRAN 887
PRINT 46, 1440          TRAN 888
PRINT 8               TRAN 889
PRINT 5, PRABT,RBTNOD,RBTRM,RBTEND,RNDEND,RBTRM2,VOLND1*FACTOR  TRAN 890
PRINT 7, IRABT,IRABT2,K1,K2  TRAN 891
PRINT 5, (VOL1(J),J=1,JJ)  TRAN 892
1460 CONTINUE          TRAN 893
C                      TRAN 894
C                      TRAN 895
1465 DO 1470 J=1,JJ          TRAN 896
1470 VSTORE(J)=VOL1(J)          TRAN 897
IF(DEBUG) GO TO 1490  TRAN 898
PRINT 46, 1470          TRAN 899
PRINT 8               TRAN 900

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PRINT 5, (VSTORE(J),J=1,JJ)          TRAN 901
PRINT 8                               TRAN 902
1490 CONTINUE                           TRAN 903
DO 1500 J=1,JJ                         TRAN 904
VINTMD(J)=VSTORE(J)*RH04(J)           TRAN 905
RH04(J)=DENSE(T(4,J))                TRAN 906
1500 VOL1(J)=VINTMD(J)/RH04(J)         TRAN 907
IF(DEBUG) GO TO 1520                  TRAN 908
PRINT 46, 1500                         TRAN 909
PRINT 8                               TRAN 910
PRINT 5, (RH04(J),J=1,JJ)              TRAN 911
PRINT 8                               TRAN 912
PRINT 5, (VOL1(J),J=1,JJ)              TRAN 913
PRINT 8                               TRAN 914
1520 CONTINUUF                         TRAN 915
DO 1530 J=1,JJ                         TRAN 916
1530 STORE(J)=T(4,J)                   TRAN 917
IF(DEBUG) GO TO 1550                  TRAN 918
PRINT 46, 1530                         TRAN 919
PRINT 4, (STORE(J),J=1,JJ)             TRAN 920
PRINT 8                               TRAN 921
1550 CONTINUE                           TRAN 922
VOLEXS=0.
DO 1600 J=2,JJ                         TRAN 923
K=JJ-J+1                            TRAN 924
VOLEXS=VOLEXS+VOL1(K+1)-VSTORE(K+1)   TRAN 925
IF(VOLEXS-FACTOR*VOLND1)1570,1560,1560
1560 PRINT 10                           TRAN 926
GO TO 100                            TRAN 927
1570 CONTINUE                           TRAN 928
T(4,K)=(VOLEXS*RHO4(K+1)*STORE(K+1)+(VSTORE(K)-VOLEXS)*RHO4(K)
X*STORE(K))/(VOLEXS*RHO4(K+1)*(VSTORE(K)-VOLEXS)*RHO4(K))   TRAN 929
IF(DEBUG) GO TO 1590                  TRAN 930
PRINT 46, 1570                         TRAN 931
PRINT 5, VOLEXS,T(4,K)                 TRAN 932
PRINT 8                               TRAN 933
1590 CONTINUE                           TRAN 934
1600 CONTINUE                           TRAN 935
VOLREP=(G1*3.1415927*(R(5)**2)*DTAU)/R40IN4               TRAN 936
DO 1610 J=1,JJ                         TRAN 937
1610 VEQIV(J)=VSTORE(J)/VSTORE(JJ)        TRAN 938
VRPEQV=VOLREP/VSTORE(JJ)                TRAN 939
DO 1620 J=1,JJ                         TRAN 940
1620 VSTORE(J)=VEQIV(J)                 TRAN 941
VADD=0.
DO 1630 J=1,JJ                         TRAN 942
K=JJ-J+1                            TRAN 943
VADD=VADD+VEQIV(K)                   TRAN 944
IF(VADD-VRPEQV)1630,1630,1640       TRAN 945
1630 CONTINUE                           TRAN 946
DO 1631 J=1,JJ                         TRAN 947
1631 T(4,J)=TMPIN4                    TRAN 948
GO TO 1780                            TRAN 949
1640 CONTINUE                           TRAN 950
VEXEQV=VADD-VRPEQV                  TRAN 951
IF(DEBUG) GO TO 1660                  TRAN 952
PRINT 46, 1640                         TRAN 953
PRINT 5, VRPEQV,VADD,VEXEQV          TRAN 954
1660 CONTINUE                           TRAN 955
DO 1670 J=1,JJ                         TRAN 956

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1670 RHO4(J)=DENSE(T(4,J))
DO 1680 J=1,JJ
1680 STORE(J)=T(4,J)
IF(DEBUG) GO TO 1700
PRINT 46, 1680
PRINT 8
PRINT 5, (RHO4(J),J=1,JJ)
PRINT 8
PRINT 4, (STORE(J),J=1,JJ)
PRINT 8
1700 CONTINUE
I20=JJ-K
KEXIT=K
DO 1710 L=1,I20
MM=JJ-L+1
T(4,MM)=TMPIN4
T(4,K)=((VEQUIV(K)-VEXEQV)*TMPIN4*RHO4*VEXEQV*STORE(JJ)*RHO4(JJ))
X/
X((VEQUIV(K)-VEXEQV)*RHO4*VEXEQV*RHO4(JJ))
I21=I20+2
VLEFT=VEQUIV(JJ)-VEXEQV
LINCRS=1
INCRS=0
DO 1770 J=I21,JJ
XNMRTR=0.
INNER=0
DENMTR=0,
K=JJ-J+1
M=K+JJ-KEXIT+LINCRS-INCRS
1720 IF(VLEFT-VEQUIV(K))1730,1760,1760
1730 XNMRTR=VLEFT*STORE(M)*RHO4(M)*XNMRTR
DENMTR=VLEFT*RHO4(M)*DENMTR
VEQUIV(K)=VEQUIV(K)-VLEFT
MINUS=M-1
VLEFT=VSTORE(MINUS)
IF(VLEFT-VEQUIV(K))1740,1740,1750
1740 IMARK=M-1-INNER
XNMRTR=VLEFT*STORE(IMARK)*RHO4(IMARK)+XNMRTR
DENMTR=VLEFT*RHO4(IMARK)*DENMTR
VEQUIV(K)=VEQUIV(K)-VLEFT
IMARK2=IMARK-1
VLEFT=VSTORE(IMARK2)
INCRS=INCRS+1
INNER=INNER+1
IF(VLEFT-VEQUIV(K))1740,1740,1750
1750 IMARK=M-1-INNER
XNMRTR=XNMRTR+VEQUIV(K)*STORE(IMARK)*RHO4(IMARK)
DENMTR=DENMTR+VEQUIV(K)*RHO4(IMARK)
T(4,K)=XNMRTR/DENMTR
VLEFT=VLEFT-VEQUIV(K)
GO TO 1770
1760 T(4,K)=STORE(M)
VLEFT=VLEFT-VEQUIV(K)
LINCRS=LINCRS+1
1770 CONTINUE
1780 IF(DEBUG) GO TO 1790
PRINT 8
PRINT 46, 1780
PRINT 4, (T(4,J),J=1,JJ)
PRINT 8
TRAN 961
TRAN 962
TRAN 963
TRAN 964
TRAN 965
TRAN 966
TRAN 967
TRAN 968
TRAN 969
TRAN 970
TRAN 971
TRAN 972
TRAN 973
TRAN 974
TRAN 975
TRAN 976
TRAN 977
TRAN 978
TRAN 979
TRAN 980
TRAN 981
TRAN 982
TRAN 983
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TRAN 986
TRAN 987
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TRAN 990
TRAN 991
TRAN 992
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TRAN 994
TRAN 995
TRAN 996
TRAN 997
TRAN 998
TRAN 999
TRAN1000
TRAN1001
TRAN1002
TRAN1003
TRAN1004
TRAN1005
TRAN1006
TRAN1007
TRAN1008
TRAN1009
TRAN1010
TRAN1011
TRAN1012
TRAN1013
TRAN1014
TRAN1015
TRAN1016
TRAN1017
TRAN1018
TRAN1019
TRAN1020

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1790	CONTINUE	TRAN1021
	GO TO 1795	TRAN1022
C		TRAN1023
C		TRAN1024
C		TRAN1025
1792	READ 2, I,I15,I16,I17,I18,I20,I21,II, XIII,IJKLMN,IMARK,IMARK2,INGRES,INNER,INTERM, XIRABT,IRABT2,J,JJ,K,K1,K2, XKEXIT,KK1,KKK2,L,LINCRS,LMN,LSTEDY, XM,MEND,MFLOW,MHEAT,MINUS,MM,MOPT, XMPOSN,MPRINT,MRVRS,MSTEDY,MSTOP,N,NN,NPRINT READ 36, DEBUG	TRAN1026
	READ 2, (IFRAC8(J),J=1,JJ)	TRAN1027
	READ 1, A,ADVNE,AXIAL,CONDAL,CPAL,D,D1,D2,	TRAN1028
XD3,DELR1,DELR2,DELR5,DELR6,DENMTR,DTAU,FACTOR, <td>TRAN1029</td>	TRAN1029	
XG1,G2,G3,GPRIMARY,GZERO,PRABT,QMAXM,QMAXW,R,RBTEND, <td>TRAN1030</td>	TRAN1030	
XRBTNOD,RBTRM,RBTRM2,REMAIN,RHOAL,RHOIN4,RHOIN8,RHRVS4,RHRVS8, <td>TRAN1031</td>	TRAN1031	
XRLNGTH,RMOVE,RNDEND,RNODE,TDEBUG,	TRAN1032	
XTFINAL,TIME,TMPIN4,TMPIN8, <td>TRAN1033</td>	TRAN1033	
XTPRINT,TRVRS4,TRVRS8,TSTART,VADD,VEXEQV,VLEFT,VOLEXS, <td>TRAN1034</td>	TRAN1034	
XVOLND1,VOLND3,VOLREP,VRPEOV,XNMRTR,ZTUBE	TRAN1035	
READ 1, (A1(J),A2(J),A3(J),A4(J),A5(J),A6(J), <td>TRAN1036</td>	TRAN1036	
XA7(J),A8(J),A9(J),A10(J),A11(J),A12(J),A13(J), <td>TRAN1037</td>	TRAN1037	
XA14(J),A15(J),A16(J),A17(J),A18(J), <td>TRAN1038</td>	TRAN1038	
XB1(J),B2(J),B3(J),B4(J),B5(J),B6(J),B7(J),B8(J), <td>TRAN1039</td>	TRAN1039	
XB9(J),B10(J),B11(J),B12(J),B13(J),B14(J),B15(J), <td>TRAN1040</td>	TRAN1040	
XCP4(J),CP8(J),DIS4(J),DIS8(J),FRAC8(J), <td>TRAN1041</td>	TRAN1041	
XHEAT(J),HL3(J),HL5(J),HL7(J),QAL(J),QALWPQ(J), <td>TRAN1042</td>	TRAN1042	
XQH20(J),QH204(J),QH208(J),HEMAN8(J),RH04(J), <td>TRAN1043</td>	TRAN1043	
XRH08(J),STORE(J),VEQUIV(J),VINTMD(J),VJL1(J), <td>TRAN1044</td>	TRAN1044	
XVOL3(J),VSTORE(J),J=1,JJ)	TRAN1045	
READ 1, (TFLLOW(J),YFLLOW(J),J=1,MFLOW)	TRAN1046	
READ 1, (TITCFLOW(J),YTITCFLOW(J),J=1,MITCFLOW)	TRAN1047	
READ 1, (THEAT(J),YHEAT(J),J=1,MHEAT)	TRAN1048	
READ 1, (TPOSN(J),YPOSN(J),J=1,MPOSN)	TRAN1049	
READ 1, ((F(LMN,J),LMN=1,8),J=1,JJ)	TRAN1050	
READ 1, ((T(LMN,J),LMN=1,8),J=1,JJ)	TRAN1051	
READ 1, (((G(LMN,L951,J),LMN=1,8),L951=1,8),J=1,JJ)	TRAN1052	
C		TRAN1053
C		TRAN1054
C		TRAN1055
1795	IF(TIMELEFT(1).LT.9500)1830,1800	TRAN1056
1830	CONTINUE	TRAN1057
	PRINT 37	TRAN1058
PUNCH 2, 2	TRAN1059	
PUNCH 2, I,I15,I16,I17,I18,I20,I21,II, XIII,IJKLMN,IMARK,IMARK2,INGRES,INNER,INTERM, XIRABT,IRABT2,J,JJ,K,K1,K2, XKEXIT,KK1,KKK2,L,LINCRS,LMN,LSTEDY, XM,MEND,MFLOW,MHEAT,MINUS,MITCFLOW,MM,MOPT, XMPOSN,MPRINT,MRVRS,MSTEDY,MSTOP,N,NN,NPRINT PUNCH 36, DEBUG	TRAN1060	
	PUNCH 2, (IFRAC8(J),J=1,JJ)	TRAN1061
	READ 1, A,ADVNE,AXIAL,CONDAL,CPAL,D,D1,D2,	TRAN1062
XD3,DELR1,DELR2,DELR5,DELR6,DENMTR,DTAU,FACTOR, <td>TRAN1063</td>	TRAN1063	
XG1,G2,G3,GPRIMARY,GZERO,PRABT,QMAXM,QMAXW,R,RBTEND, <td>TRAN1064</td>	TRAN1064	
XRBTNOD,RBTRM,RBTRM2,REMAIN,RHOAL,RHOIN4,RHOIN8,RHRVS4,RHRVS8, <td>TRAN1065</td>	TRAN1065	
XRLNGTH,RMOVE,RNDEND,RNODE,TDEBUG,	TRAN1066	
XTFINAL,TIME,TMPIN4,TMPIN8, <td>TRAN1067</td>	TRAN1067	
XTPRINT,TRVRS4,TRVRS8,TSTART,VADD,VEXEQV,VLEFT,VOLEXS, <td>TRAN1068</td>	TRAN1068	
		TRAN1069
		TRAN1070
		TRAN1071
		TRAN1072
		TRAN1073
		TRAN1074
		TRAN1075
		TRAN1076
		TRAN1077
		TRAN1078
		TRAN1079
		TRAN1080

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*XVOLND1,VOLND3,VOLREP,VHPEQV,XNMRTR,ZTUBE
PUNCH 1, (A1(J),A2(J),A3(J),A4(J),A5(J),A6(J),
XA7(J),AB(J),A9(J),A10(J),A11(J),A12(J),A13(J),
XA14(J),A15(J),A16(J),A17(J),A18(J),
XB1(J),B2(J),B3(J),B4(J),B5(J),B6(J),B7(J),B8(J),
XB9(J),B10(J),B11(J),B12(J),B13(J),B14(J),B15(J),
XCP4(J),CP8(J),DIS4(J),DIS8(J),FRAC8(J),
XHEAT(J),HL3(J),HL5(J),HL7(J),QAL(J),QALWPG(J),
XQH20(J),QH204(J),QH208(J),HEMAN8(J),RH04(J),
XRHO8(J),STORE(J),VEQUIV(J),VINTMD(J),VOL1(J),
XVOL3(J),VSTORE(J),J=1,JJ)
PUNCH 1, (TFLOW(J),YFLW(J),J=1,MFLOW)
PUNCH 1, (TITCFLOW(J),YITCFLOW(J),J=1,MITCFLOW)
PUNCH 1, (THEAT(J),YHEAT(J),J=1,MHEAT)
PUNCH 1, (TPOSN(J),YPOSN(J),J=1,MPOSN)
PUNCH 1, ((F(LMN,J),LMN=1,8),J=1,JJ)
PUNCH 1, ((T(LMN,J),LMN=1,8),J=1,JJ)
PUNCH 1, (((G(LMN,L951,J),LMN=1,8),L951=1,8),J=1,JJ)
GO TO 1850
1800 CONTINUE
GO TO 1805
1802 READ 2, I,I15,I16,I17,I18,I20,I21,II,
XIII,IJKLMN,IMARK,IMARK2,INGRES,INNER,INTERM,
XIRABT,IRABT2,J,JJ,K,K1,K2,
XKEXIT,KK1,KKK2,L,LINERS,LMN,LSTEDY,
XM,MEND,MFLOW,MHEAT,MINUS,MITCFLOW,MM,MDPT,
XMPSON,MPRINT,MRVRS,MSTEDY,MSTOP,N,NN,NPRINT
READ 36, DEBUG
READ 2, (IFRAC8(J),J=1,JJ)
READ 1, A,ADVNE,AXIAL,CONDUAL,CPAL,D,D1,D2,
XD3,DELR1,DELR2,DELR5,DELR6,DENMTR,DTAU,FACTOR,
XG1,G2,G3,GPRIMARY,GZERO,PRABT,QMAXM,QMAXW,R,RBTEND,
XRBTND,RBTRM,RBTRM2,REMAIN,RHOAL,RHOIN4,RHOIN8,RHRS4,RHRS8,
XRLNGTH,RMOVE,RNDEND,RNDE,DEBUG,
XTFINAL,TIME,TMPIN4,TMPIN8,
XTPRINT,TRVRSS4,TRVRSS8,TSTART,VADD,VEXEQV,VLEFT,VOLEXS,
XVOLND1,VOLND3,VOLREP,VHPEQV,XNMRTR,ZTUBE
READ 1, (A1(J),A2(J),A3(J),A4(J),A5(J),A6(J),
XA7(J),AB(J),A9(J),A10(J),A11(J),A12(J),A13(J),
XA14(J),A15(J),A16(J),A17(J),A18(J),
XB1(J),B2(J),B3(J),B4(J),B5(J),B6(J),B7(J),B8(J),
XB9(J),B10(J),B11(J),B12(J),B13(J),B14(J),B15(J),
XCP4(J),CP8(J),DIS4(J),DIS8(J),FRAC8(J),
XHEAT(J),HL3(J),HL5(J),HL7(J),QAL(J),QALWPG(J),
XQH20(J),QH204(J),QH208(J),HEMAN8(J),RH04(J),
XRHO8(J),STORE(J),VEQUIV(J),VINTMD(J),VOL1(J),
XVOL3(J),VSTORE(J),J=1,JJ)
READ 1, (TFLOW(J),YFLW(J),J=1,MFLOW)
READ 1, (TITCFLOW(J),YITCFLOW(J),J=1,MITCFLOW)
READ 1, (THEAT(J),YHEAT(J),J=1,MHEAT)
READ 1, (TPOSN(J),YPOSN(J),J=1,MPOSN)
READ 1, ((F(LMN,J),LMN=1,8),J=1,JJ)
READ 1, ((T(LMN,J),LMN=1,8),J=1,JJ)
READ 1, (((G(LMN,L951,J),LMN=1,8),L951=1,8),J=1,JJ)
READ 1, TFINAL
1805 IF(TPRINT-TFINAL)>300,1810,1810
1810 CONTINUE
PUNCH 2, 1
PUNCH 2, I,I15,I16,I17,I18,I20,I21,II,
XIII,IJKLMN,IMARK,IMARK2,INGRES,INNER,INTERM,

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XIRABT,IRABT2,J,JJ,K,K1,K2,          TRAN1141
XKEXIT,KK1,KKK2,L,LINCRS,LMN,LSTEDY,  TRAN1142
XM,MEND,MFLOW,MHEAT,MINUS,MTCFLOW,MM,MJPT,  TRAN1143
XMPOSN,MPRINT,MRVRS,MSTEDY,MSTOP,N,NN,NPRINT  TRAN1144
PUNCH 36, DEBUG                      TRAN1145
PUNCH 2, (IFRAC8(J),J=1,JJ)          TRAN1146
PUNCH 1, A,ADVNC,EAXIAL,CONDAL,CPAL,D,D1,D2,  TRAN1147
XD3,DELR1,DELR2,DELR5,DELR6,DENMTR,DTAU,FACTOR,  TRAN1148
XG1,G2,G3,GPRIMARY,GZERO,PRABT,QMAXM,QMAXW,R,RBTEND,  TRAN1149
XRRTNOD,RBTRM,RBTRM2,REMAIN,RHOAL,RHOIN4,RHOIN8,RHRVS4,RHRVS8,  TRAN1150
XRLNGTH,RMOVE,RNDEND,RNODE,TDEBUG,  TRAN1151
XTFINAL,TIME,TMPIN4,TMPIN8,  TRAN1152
XTPRINT,TRVRS4,TRVRS8,TSTART,VADD,VEXEQV,VLEFT,VOLEXS,  TRAN1153
XVOLND1,VOLREP,VRPEQV,XNMRTZTUBE  TRAN1154
PUNCH 1, (A1(J),A2(J),A3(J),A4(J),A5(J),A6(J),  TRAN1155
XA7(J),A8(J),A9(J),A10(J),A11(J),A12(J),A13(J),  TRAN1156
XA14(J),A15(J),A16(J),A17(J),A18(J),  TRAN1157
XB1(J),B2(J),B3(J),B4(J),B5(J),B6(J),B7(J),B8(J),  TRAN1158
XB9(J),B10(J),B11(J),B12(J),B13(J),B14(J),B15(J),  TRAN1159
XCP4(J),CP8(J),DIS4(J),DIS8(J),FRAC8(J),  TRAN1160
XHEAT(J),HL3(J),HL5(J),HL7(J),QAL(J),QALWPQ(J),  TRAN1161
XGH20(J),QH204(J),QH208(J),REMAB(J),RH04(J),  TRAN1162
XRH08(J),STORE(J),VEQUIV( ),VINTMD(J),VOL1(J),  TRAN1163
XVOL3(J),VSTORE(J),J=1,JJ)          TRAN1164
PUNCH 1, (TFLOW(J),YFLOW(J),J=1,MFLOW)  TRAN1165
PUNCH 1, (TITCFLOW(J),YITCFLOW(J),J=1,MTCFLOW)  TRAN1166
PUNCH 1, (THEAT(J),YHEAT(J),J=1,MHEAT)  TRAN1167
PUNCH 1, (TPOSN(J),YPSN(J),J=1,MPOSN)  TRAN1168
PUNCH 1, ((F(LMN,J),LMN=1,8),J=1,JJ)  TRAN1169
PUNCH 1, ((T(LMN,J),LMN=1,8),J=1,JJ)  TRAN1170
PUNCH 1, (((G(LMN,L951,J),LMN=1,8),L951=1,8),J=1,JJ)  TRAN1171
PRINT 14                           TRAN1172
GO TO 100                          TRAN1173
1850 END                          TRAN1174

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SUBROUTINE STEADY

THIS SUBROUTINE IS USED TO DETERMINE THE STEADY-STATE TEMPERATURE MAP OF A HYDRAULIC RABBIT ASSEMBLY.

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C STEA 1
C STEA 2
C STEA 3
C STEA 4
C STEA 5
DIMENSION A1(50),A2(50),A3(50),A4(50),A5(50),A6(50),A7(50),A8(50),STEA 6
XA9(50),A10(50),A11(50),A12(50),A13(50),A14(50),A15(50),STEA 7
XB1(50),B2(50),B3(50),B4(50),B5(50),B6(50),B7(50),B8(50),B9(50),STEA 8
XB10(50),B11(50),B12(50),STEA 9
XCP4(50),CP8(50),STEA 10
XF(50),STEA 11
XG(8,8),STEA 12
XHEAT(50),HL3(50),HL5(50),HL7(50),STEA 13
XQALWP(50),QALWPG(50),QH20(50),QH204(50),QH208(50),STEA 14
XR(8),RH04(50),RH08(50),STEA 15
XT(8,50),TFLW(50),THEAT(50),TITCFLOW(50),STEA 16
XYFLOW(50),YHEAT(50),YITCFLOW(50),STEA 17
TYPE LOGICAL DEBUG STEA 18
COMMON/1/DEBUG/2/TIME,BLANK1(101)/4/TFLW,YFLW,MFLW,
XGPRIMARY,G1,G2,STEA 19
XG3,GZERO/5/R/8/RNODE,RLNGTH,RH04,BLANK2(4)/9/T/10/JJ,K1,K2,KK1,STEA 20
XKKK2/11/HEAT,THEAT,YHEAT,QH20,QALWPG,QMAXW,QMAXM/12/MHEAT STEA 21
X/14/CONDAL,RHOAL,CP4,CP8,RH08,HL5,HL7,D1,D2,D3,DELR1,DELR2,STEA 22
XDELR5,DELR6,RBTM,RBTMR2,TMPIN4,TMPIN8 STEA 23
COMMON/17/MTCFLOW,TITCFLOW,YITCFLOW STEA 24
1 FORMAT(10E12.5) STEA 25
2 FORMAT(10I12) STEA 26
3 FORMAT(36X,7F12.4) STEA 27
4 FORMAT(10F12.4) STEA 28
5 FORMAT(57H THE INITIAL CONDITION, STEADY-STATE TEMPERATURE MAP***STEA 30
X*//)
6 FORMAT(1H1,17HSUBROUTINE STEADY//) STEA 31
7 FORMAT(1X,I3) STEA 32
8 FORMAT(/) STEA 33
9 FORMAT(1X,I5) STEA 34
10 FORMAT(12X,STEA 35
X 97H THE DEBUG OPTION WILL BE USED IN THIS PROBLEM WHEN DETESTEA 36
X REMINING THE STEADY-STATE TEMPERATURE MAP./) STEA 37
IF(DEBUG)GO TO 100 STEA 38
PRINT 6 STEA 39
PRINT 10 STEA 40
100 CONTINUE STEA 41
LPASS=0 STEA 42
LPASS9=0 STEA 43
IF(DEBUG)GO TO 110 STEA 44
PRINT 9, 100 STEA 45
PRINT 1, R,CONDAL,DELR1,DELR2,DELR5,DE_R6,RNODE,((T(I,J),I=1,8),
XJ=1,JJ),(TFLW(I),I=1,MFLW),(YFLW(I),I=1,MFLW),GPRIMARY,G1,G2,STEA 46
XG3,STEA 47
XGZERO,D1,(HL5(I),I=1,JJ),(RH04(I),I=1,JJ),(CP4(I),I=1,JJ),D3,
X(HL7(I),I=1,JJ),(RH08(I),I=1,JJ),(CP8(I),I=1,JJ),QMAXW,QMAXM,STEA 48
X(HEAT(I),I=1,JJ),(THEAT(I),I=1,MHEAT),(YHEAT(I),I=1,MHEAT),
X(QH20(I),I=1,JJ),(QALWPG(I),I=1,JJ),TMPIN4,TMPIN8,RHOAL STEA 49
PRINT 2, MFLW,JJ,MHEAT STEA 50
110 CALL FLOW STEA 51
CALL QHEAT STEA 52
IF(DEBUG)GO TO 120 STEA 53
PRINT 8 STEA 54
PRINT 9, 110 STEA 55
PRINT 1, (TFLW(I),I=1,MFLW),(YFLW(I),I=1,MFLW),GPRIMARY,R(3),STEA 56

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XR(5),G1,G2,G3,GZERO
PRINT 2, MFLOW
120 L=JJ-KKK2
DO 310 K=1,L
130 J=JJ-K+1
140 CONTINUE
IF(DEBUG)GO TO 150
PRINT 8
PRINT 9, 140
PRINT 2, K,J,JJ,MHEAT
PRINT 1, QMAXW,QMAXM,(HEAT(I),I=1,JJ),(THEAT(I),I=1,MHEAT),
X(YHEAT(I),I=1,MHEAT),(QH20(I),I=1,JJ),(QALWPG(I),I=1,JJ)
150 QAL(J)=1551.0774*RHOAL*QALWPG(J)
A5(J)=4.*CONDAL*(2.*R(5)+DELR5)
A6(J)=(DELR5**2)*QAL(J)*(4.*R(5)+DELR5)
A7(J)=CONDAL*(2.*R(6)-DELR5)
A8(J)=CONDAL*(2.*R(6)+DELR6)
A9(J)=2.*R(6)*(DELR6**2)*QAL(J)
A10(J)=4.*CONDAL*(2.*R(7)-DELR6)
A12(J)=(DELR6**2)*QAL(J)*(4.*R(7)-DELR6)
IF(DEBUG)GO TO 160
PRINT 8
PRINT 9, 150
PRINT 1, QAL(J),A5(J),A6(J),A7(J),A8(J),A9(J),A10(J),A12(J)
160 INDEX=1
170 CALL WATER(T(4,J),D1,G1,HL5(J),RH04(J),CP4(J))
CALL WATER(T(8,J),D3,G3,HL7(J),RH08(J),CP8(J))
IF(DEBUG)GO TO 180
PRINT 8
PRINT 9, 170
PRINT 1, T(4,J),D1,G1,HL5(J),RH04(J),CP4(J),T(8,J),D3,G3,
XHL7(J),RH08(J),CP8(J)
180 QH204(J)=1551.0774*RHO4(J)*QH20(J)
QH208(J)=1551.0774*RHO8(J)*QH20(J)
A1(J)=2.*HL5(J)
IF(LPASS)190,190,200
190 A2(J)=R(5)*QH204(J)
GO TO 210
200 A2(J)=R(5)*((1.-RBTRM2)*QH204(J)+RBTRM2*((((R(5)**2=R(3)**2)/
XR(5)**2)*QH204(J)+(R(5)**2)/(R(5)**2))*QAL(J)))
210 A3(J)=R(5)*ABSF(G1)*CP4(J)/RNODE
A4(J)=8.*R(5)*DELR5*HL5(J)
A11(J)=8.*HL7(J)*R(7)*DELR6
A13(J)=2.*R(7)*HL7(J)
A14(J)=(R(8)**2=R(7)**2)*QH208(J)
A15(J)=(R(8)**2=R(7)**2)*ABSF(G3)*CP8(J)/RNODE
IF(DEBUG)GO TO 220
PRINT 8
PRINT 9, 210
PRINT 1, QH204(J),QH208(J),A1(J),A2(J),A3(J),A4(J),A11(J),A13(J),
XA14(J),A15(J)
220 IF(K-1)230,230,240
230 F(1)=-A2(J)-A3(J)*TMPIN4
F(5)=-A14(J)-A15(J)*TMPIPN8
GO TO 250
240 F(1)=-A2(J)-A3(J)*T(4,J+1)
F(5)=-A14(J)-A15(J)*T(8,J+1)
250 F(2)=-A6(J)
F(3)=-A9(J)
F(4)=-A12(J)

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IF(DEBUG)GO TO 260
PRINT 8
PRINT 9, 250
PRINT 1, (F(I),I=1,5)
260 G(1,1)=A1(J)-A3(J)
G(1,2)=A1(J)
G(2,1)=A4(J)
G(2,2)=A4(J)-A5(J)
G(2,3)=A5(J)
G(3,2)=A7(J)
G(3,3)=A7(J)-A8(J)
G(3,4)=A8(J)
G(4,3)=A10(J)
G(4,4)=A10(J)-A11(J)
G(4,5)=A11(J)
G(5,4)=A13(J)
G(5,5)=A13(J)-A15(J)
IF(DEBUG)GO TO 270
PRINT 8
PRINT 9, 260
PRINT 1, G(1,1),G(1,2),G(2,1),G(2,2),G(2,3),G(3,2),G(3,3),G(3,4),
XG(4,3),G(4,4),G(4,5),G(5,4),G(5,5)
270 CALL GAUSS1(G,5,F)
IF(DEBUG)GO TO 280
PRINT 8
PRINT 9, 270
PRINT 1, (F(I),I=1,5)
280 DO 290 N=1,5
NN=N+3
290 T(NN,J)=F(N)
IF(DEBUG)GO TO 300
PRINT 9, 290
PRINT 3, (T(LMN,J),LMN=4,8)
300 INDEX=INDEX+1
IF(INDEX=5)170,170,310
310 CONTINUE
IF(LPASS)320,320,340
320 IF(RBTRM2=.5)330,330,340
330 J=J+1
LPASS=1
GO TO 140
340 CONTINUE
L8=JJ-J+2
L9=JJ-KK1
IF(DEBUG)GO TO 350
PRINT 8
PRINT 9, 340
PRINT 2, L8,L9
350 DO 530 K=L8,L9
J=JJ-K+1
360 CONTINUE
IF(DEBUG)GO TO 370
PRINT 8
PRINT 9, 360
PRINT 2, K,J,JJ,MHEAT
PRINT 1, QMAXW,QMAXM,(HEAT(I),I=1,JJ),(THEAT(I),I=1,MHEAT),
X(YHEAT(I),I=1,MHEAT),(QH20(I),I=1,JJ),(QALWPG(I),I=1,JJ)
370 QAL(J)=1551.0774*RHOAL*QALWPG(J)
A5(J)=4.*CONDAL*(2.*R(5)*DELR5)
A6(J)=(DELR5**2)*QAL(J)*(4.*R(5)*DELR5)
STEA 121
STEA 122
STEA 123
STEA 124
STEA 125
STEA 126
STEA 127
STEA 128
STEA 129
STEA 130
STEA 131
STEA 132
STEA 133
STEA 134
STEA 135
STEA 136
STEA 137
STEA 138
STEA 139
STEA 140
STEA 141
STEA 142
STEA 143
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STEA 171
STEA 172
STEA 173
STEA 174
STEA 175
STEA 176
STEA 177
STEA 178
STEA 179
STEA 180

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A7(J)=CONDAL*(2.*R(6)-DELR5) STEA 181
A8(J)=CONDAL*(2.*R(6)+DELR6) STEA 182
A9(J)=2.*R(6)*(DELR6**2)*QAL(J) STEA 183
A10(J)=4.*CONDAL*(2.*R(7)-DELR6) STEA 184
A12(J)=(DELR6**2)*QAL(J)*(4.*R(7)-DELR6) STEA 185
B1(J)=4.*CONDAL STEA 186
B2(J)=(DELR1**2)*QAL(J) STEA 187
B3(J)=CONDAL*(2.*R(2)-DELR1) STEA 188
B4(J)=CONDAL*(2.*R(2)+DELR2) STEA 189
B5(J)=2.*R(2)*(DELR1**2)*QAL(J) STEA 190
B6(J)=4.*CONDAL*(2.*R(3)-DELR2) STEA 191
B8(J)=(DELR2**2)*(4.*R(3)-DELR2)*QAL(J) STEA 192
IF(DEBUG)GO TO 380 STEA 193
PRINT 8 STEA 194
PRINT 9, 370 STEA 195
PRINT 1, QAL(J),A5(J),A6(J),A7(J),A8(J),A9(J),A10(J),A12(J) STEA 196
X,B1(J),B2(J),B3(J),B4(J),B5(J),B6(J),BB(J) STEA 197
380 INDEX1 STEA 198
390 CALL WATER(T(4,J),D2,G2,HL5(J),RH04(J),CP4(J)) STEA 199
CALL WATER(T(8,J),D3,G3,HL7(J),RH08(J),CP8(J)) STEA 200
HL3(J)=HL5(J) STEA 201
IF(DEBUG)GO TO 400 STEA 202
PRINT 8 STEA 203
PRINT 9, 390 STEA 204
PRINT 1, T(4,J),D2,G2,HL3(J),RH04(J),CP4(J),T(8,J),D3,G3, STEA 205
XHL7(J),RH08(J),CP8(J) STEA 206
400 QH204(J)=1551.0774*RH04(J)*QH20(J) STEA 207
QH208(J)=1551.0774*RH08(J)*QH20(J) STEA 208
A4(J)=8.*R(5)*DELR5*HL5(J) STEA 209
A11(J)=8.*HL7(J)*R(7)*DELR6 STEA 210
A13(J)=2.*R(7)*HL7(J) STEA 211
A14(J)=(R(8)**2-R(7)**2)*QH208(J) STEA 212
A15(J)=(R(8)**2-R(7)**2)*G3*CP8(J)/RNODE STEA 213
B7(J)=8.*DELR2*HL3(J)*R(3) STEA 214
B9(J)=2.*HL3(J)*R(3) STEA 215
B10(J)=2.*HL5(J)*R(5) STEA 216
B11(J)=(R(5)**2-R(3)**2)*QH204(J) STEA 217
B12(J)=(R(5)**2-R(3)**2)*ABSF(G2)*CP4(J)/RNODE STEA 218
IF(DEBUG)GO TO 410 STEA 219
PRINT 8 STEA 220
PRINT 9, 400 STEA 221
PRINT 1, QH204(J),QH208(J),A1(J),A2(J),A3(J),A4(J),A11(J),A13(J), STEA 222
XA14(J),A15(J) STEA 223
X,B7(J),B9(J),B10(J),B11(J),B12(J) STEA 224
410 IF(LPASS9)420,420,440 STEA 225
420 IF(LPASS9)430,430,470 STEA 226
430 QFIX = ((1.-RBTRM2)*QH204(J)+RBTRM2*((((R(5)**2-R(3)**2)/
XR(5)**2)*QH204(J)+((R(3)**2)/(R(5)**2))*QAL(J))) STEA 227
LPASS=1 STEA 228
GO TO 450 STEA 229
440 QFIX=(RBTRM*QH204(J)+(1.-RBTRM)*(((R(5)**2-R(3)**2)/
XR(5)**2)*QH204(J)+((R(3)**2)/(R(5)**2))*QAL(J))) STEA 230
STEA 231
450 B2(J)=(DELR1**2)*QFIX STEA 232
B5(J)=2.*R(2)*(DELR1**2)*QFIX STEA 233
B8(J)=(DELR2**2)*(4.*R(3)-DELR2)*QFIX STEA 234
IF(DEBUG)GO TO 460 STEA 235
PRINT 8 STEA 236
PRINT 9, 450 STEA 237
PRINT 1, B2(J),B5(J),B8(J) STEA 238
460 CONTINUE STEA 239
STEA 240

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470 CONTINUE
F(1)=-B2(J)
F(2)=-B5(J)
F(3)=-B8(J)
F(4)=-B11(J)-B12(J)*T(4,J+1)
F(5)=-A6(J)
F(6)=-A9(J)
F(7)=-A12(J)
F(8)=-A14(J)-A15(J)*T(8,J+1)
IF(DEBUG)GO TO 480
PRINT 8
PRINT 9, 470
PRINT 1, (F(I),I=1,8)
480 G(1,1)=-B1(J)
G(1,2)=B1(J)
G(2,1)=B3(J)
G(2,2)=-B3(J)-B4(J)
G(2,3)=B4(J)
G(3,2)=B6(J)
G(3,3)=-B6(J)-B7(J)
G(3,4)=R7(J)
G(4,3)=B9(J)
G(4,4)=-B9(J)-B10(J)-B12(J)
G(4,5)=B10(J)
G(5,4)=A4(J)
G(5,5)=-A4(J)-A5(J)
G(5,6)=A5(J)
G(6,5)=A7(J)
G(6,6)=-A7(J)-A8(J)
G(6,7)=A8(J)
G(7,6)=A10(J)
G(7,7)=-A10(J)-A11(J)
G(7,8)=A11(J)
G(8,7)=A13(J)
G(8,8)=-A13(J)-A15(J)
IF(DEBUG)GO TO 490
PRINT 8
PRINT 9, 480
PRINT 1, G(1,1),G(1,2),G(2,1),G(2,2),G(2,3),G(3,2),G(3,3),G(3,4),
XG(4,3),G(4,4),G(4,5),G(5,4),G(5,5),G(5,6),G(6,5),G(6,6),G(6,7),
XG(7,6),G(7,7),G(7,8),G(8,7),G(8,8)
490 CALL GAUSS1(G,8,F)
IF(DEBUG)GO TO 500
PRINT 8
PRINT 9, 490
PRINT 1, (F(I),I=1,8)
500 DO 510 N=1,8
510 T(N,J)=F(N)
IF(DEBUG)GO TO 520
PRINT 9, 510
PRINT 4, (T(LMN,J),LMN=1,8)
520 INDEX*INDEX+1
IF(INDEX=5)390,390,530
530 CONTINUE
IF(LPASS9)540,540,560
540 IF(RBTMR-.5)550,560,560
550 J=J-1
LPASS9=1
GO TO 360
560 CONTINUE
STE A 241
STE A 242
STE A 243
STE A 244
STE A 245
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STE A 252
STE A 253
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STE A 298
STE A 299
STE A 300

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L88=JJ-J+2                      STEA 301
L99=JJ                         STEA 302
DO 700 K=L88,L99                 STEA 303
J=JJ-K+1                        STEA 304
IF(DEBUG)GO TO 570                STEA 305
PRINT 8                          STEA 306
PRINT 9, 560                     STEA 307
PRINT 2, K,J,JJ,MHEAT           STEA 308
PRINT 1, QMAXW,QMAXM,(HEAT(I),I=1,JJ),(THEAT(I),I=1,MHEAT),
X(YHEAT(I),I=1,MHEAT),(QH20(I),I=1,JJ),(QALWPG(I),I=1,JJ)    STEA 309
570 QAL(J)=1551.0774*RHOAL*QALWPG(J)    STEA 310
A5(J)=4.*CONDAL*(2.*R(5)*DELR5)      STEA 311
A6(J)=(DELR5**2)*QAL(J)*(4.*R(5)+DELR5)  STEA 312
A7(J)=CONDAL*(2.*R(6)-DELR5)        STEA 313
A8(J)=CONDAL*(2.*R(6)+DELR6)        STEA 314
A9(J)=2.*R(6)*(DELR6**2)*QAL(J)     STEA 315
A10(J)=4.*CONDAL*(2.*R(7)-DELR6)    STEA 316
A12(J)=(DELR6**2)*QAL(J)*(4.*R(7)-DELR5)  STEA 317
IF(DEBUG)GO TO 580                  STEA 318
PRINT 8                          STEA 319
PRINT 9, 570                     STEA 320
PRINT 1, QAL(J),A5(J),A6(J),A7(J),AB(J),A9(J),A10(J),A12(J)  STEA 321
580 INDEX=1                      STEA 322
590 CALL WATER(T(4,J),D1,G1,HL5(J),RH04(J),CP4(J))          STEA 323
CALL WATER(T(8,J),D3,G3,HL7(J),RH08(J),CP8(J))          STEA 324
IF(DEBUG)GO TO 600                  STEA 325
PRINT 8                          STEA 326
PRINT 9, 590                     STEA 327
PRINT 1, T(4,J),D1,G1,HL5(J),RH04(J),CP4(J),T(8,J),D3,G3,
XHL7(J),RH08(J),CP8(J)            STEA 328
600 QH204(J)=1551.0774*RH04(J)*QH20(J)          STEA 329
QH208(J)=1551.0774*RH08(J)*QH20(J)          STEA 330
A1(J)=2.*HL5(J)                   STEA 331
IF(LPASS9)620,620,610             STEA 332
610 A2(J)=R(5)*QH204(J)          STEA 333
GO TO 630                         STEA 334
620 A2(J)=R(5)*((RBTRM)*QH204(J)+(1,-RBTRM)*((R(5)**2=R(3)**2)/
X(R(5)**2)*QH204(J)+((R(3)**2)/(R(5)**2))*QAL(J)))  STEA 335
LPASS9#1                         STEA 336
630 A3(J)=R(5)*ABSF(G1)*CP4(J)/RNODE          STEA 337
A4(J)=8.*R(5)*DELR5*HL5(J)          STEA 338
A11(J)=8.*HL7(J)*R(7)*DELR6       STEA 339
A13(J)=2.*R(7)*HL7(J)             STEA 340
A14(J)=(R(8)**2=R(7)**2)*QH208(J)  STEA 341
A15(J)=(R(8)**2=R(7)**2)*ABSF(G3)*CP8(J)/RNODE          STEA 342
IF(DEBUG)GO TO 640                  STEA 343
PRINT 8                          STEA 344
PRINT 9, 630                     STEA 345
PRINT 1, QH204(J),QH208(J),A1(J),A2(J),A3(J),A4(J),A11(J),A13(J),
XA14(J),A15(J)                   STEA 346
640 F(1)=-A2(J)-A3(J)*T(4,J+1)          STEA 347
F(5)=-A14(J)-A15(J)*T(8,J+1)          STEA 348
F(2)=-A6(J)                        STEA 349
F(3)=-A9(J)                        STEA 350
F(4)=-A12(J)                       STEA 351
IF(DEBUG)GO TO 650                  STEA 352
PRINT 8                          STEA 353
PRINT 9, 640                     STEA 354
PRINT 1, (F(I),I=1,5)              STEA 355
650 G(1,1)=-A1(J)-A3(J)            STEA 356
                                         STEA 357
                                         STEA 358
                                         STEA 359
                                         STEA 360

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G(1,2)=A1(J) STEA 361
G(2,1)=A4(J) STEA 362
G(2,2)=-A4(J)-A5(J) STEA 363
G(2,3)=A5(J) STEA 364
G(3,2)=A7(J) STEA 365
G(3,3)=-A7(J)-A8(J) STEA 366
G(3,4)=A8(J) STEA 367
G(4,3)=A10(J) STEA 368
G(4,4)=-A10(J)-A11(J) STEA 369
G(4,5)=A11(J) STEA 370
G(5,4)=A13(J) STEA 371
G(5,5)=-A13(J)-A15(J) STEA 372
IF(DEBUG)GO TO 660 STEA 373
PRINT 8 STEA 374
PRINT 9, 650 STEA 375
PRINT 1, G(1,1),G(1,2),G(2,1),G(2,2),G(2,3),G(3,2),G(3,3),G(3,4), STEA 376
XG(4,3),G(4,4),G(4,5),G(5,4),G(5,5) STEA 377
660 CALL GAUSS1(G,5,F) STEA 378
IF(DEBUG)GO TO 670 STEA 379
PRINT 8 STEA 380
PRINT 9, 660 STEA 381
PRINT 1, (F(I),I=1,5) STEA 382
670 DO 680 NM=1,5 STEA 383
NN=N+3 STEA 384
680 T(NN,J)=F(N) STEA 385
IF(DEBUG)GO TO 690 STEA 386
PRINT 9, 680 STEA 387
PRINT 3, (T(LMN,J),LMN=4,8) STEA 388
690 INDEX=INDEX+1 STEA 389
IF(INDEX-5)590,590,700 STEA 390
700 CONTINUE STEA 391
PRINT 8 STEA 392
PRINT 8 STEA 393
PRINT 5 STEA 394
K1=KK1+1 STEA 395
K2=KKK2-1 STEA 396
DO 710 K=KKK2,JJ STEA 397
J=JJ+KKK2-K STEA 398
710 PRINT 3, (T(LMN,J),LMN=4,8) STEA 399
DO 720 K=K1,K2 STEA 400
J=K2+K1-K STEA 401
720 PRINT 4, (T(LMN,J),LMN=1,8) STEA 402
DO 730 K=1,KK1 STEA 403
J=KK1+1-K STEA 404
730 PRINT 3, (T(LMN,J),LMN=4,8) STEA 405
PRINT 8 STEA 406
PRINT 8 STEA 407
RETURN STEA 408
END STEA 409

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SUBROUTINE FLOW

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C THIS SUBROUTINE IS USED TO DETERMINE THE TIME-DEPENDENT WATER FLOW FLOW 1
C RATE IN THE RABBIT TUBE WATER. FLOW 2
C FLOW 3
C FLOW 4
C FLOW 5
C FLOW 6
C FLOW 7
C FLOW 8
C FLOW 9
C FLOW 10
C FLOW 11
C FLOW 12
C FLOW 13
C FLOW 14
C FLOW 15
C FLOW 16
C FLOW 17
C FLOW 18
C FLOW 19
C FLOW 20
C FLOW 21
C FLOW 22
C FLOW 23
C FLOW 24
C FLOW 25
C FLOW 26
C FLOW 27
C FLOW 28
C FLOW 29
C FLOW 30
C FLOW 31
C FLOW 32
C FLOW 33
C FLOW 34
C FLOW 35

DIMENSION X(50),
XY(50)
COMMON/2/TIME,BLANK1(101)/4/X,Y,M,GPRIMARY,G1,G2,G3,GZERO/5/R(8) FLOW
R3=R(3) $ R5=R(5)
1 FORMAT(23H0INDEPENDENT VARIABLE (,E12.5,1X,
X37H) OUT OF RANGE...,PROBLEM TERMINATED/) FLOW
CALL PRIMARY FLOW
IF(TIME>180*99.99 FLOW
99 CONTINUE FLOW
N=2 FLOW
IF(X(1)-TIME*3600.)>110,100,160 FLOW
100 G1=Y(1) FLOW
GO TO 170 FLOW
110 IF(TIME>3600.,-X(M))>120,120,160 FLOW
120 IF(TIME>3600.,-X(N))>130,140,150 FLOW
130 G1=((TIME+3600.-X(N-1))/(X(N)-X(N-1)))*(Y(N)-Y(N-1))+Y(N-1) FLOW
GO TO 170 FLOW
140 G1=Y(N) FLOW
GO TO 170 FLOW
150 N=N+1 FLOW
GO TO 110 FLOW
160 TPRINT=TIME*3600. FLOW
PRINT 1, TPRINT FLOW
TIME=-20. FLOW
GO TO 180 FLOW
170 G1=G1*GZERO FLOW
G2=G1*(R5**2/(R5**2-R3**2)) FLOW
180 CONTINUE FLOW
RETURN FLOW
END FLOW

```

SUBROUTINE PRIMARY

THIS SURROUTINE IS USED TO DETERMINE THE TIME-DEPENDENT WATER FLOW	PRIM	1
RATE IN THE WATER CELL SURROUNDING THE RABBIT TUBE.	PRIM	3
	PRIM	4
	PRIM	5
DIMENSION X(50),Y(50)	PRIM	6
DIMENSION XPRIMARY(50),YPRIAMRY(50)	PRIM	7
COMMON/2/TIME,BLANK1(101)/4/X,Y,M,GPRIMARY,G1,32,G3,GZERO/5/R(8)	PRIM	8
COMMON/17/MPRIMARY,XPRIMARY,YPRIAMRY	PRIM	9
1 FORMAT(23H0INDEPENDENT VARIABLE (,E12.5,1X,	PRIM	10
X37H) OUT OF RANGE...,,PROBLEM TERMINATED/)	PRIM	11
N=2	PRIM	12
IF(XPRIMARY(1)-TIME*3600.,)110,100,160	PRIM	13
100 G3=YPRIAMRY(1)	PRIM	14
GO TO 170	PRIM	15
110 IF(TIME*3600.-XPRIMARY(MPRIMARY))120,120,160	PRIM	16
120 IF(TIME*3600.-XPRIMARY(N))130,140,150	PRIM	17
130 G3=((TIME*3600.-XPRIMARY(N-1))/(XPRIMARY(N)-XPRIMARY(N-1)))	PRIM	18
X*(YPRIAMRY(N)-YPRIAMRY(N-1))+YPRIAMRY(N-1)	PRIM	19
GO TO 170	PRIM	20
140 G3=YPRIAMRY(N)	PRIM	21
GO TO 170	PRIM	22
150 N=N+1	PRIM	23
GO TO 110	PRIM	24
160 TPRINT=TIME*3600.	PRIM	25
PRINT 1, TPRINT	PRIM	26
TIME=-20.	PRIM	27
GO TO 180	PRIM	28
170 G3=G3*GPRIMARY	PRIM	29
180 CONTINUE	PRIM	30
RETURN	PRIM	31
END	PRIM	32

SUBROUTINE REVRSE

C THIS SUBROUTINE IS USED TO DETERMINE THE FLOW-REVERSAL WATER  
C TEMPERATURE ADJUSTMENT IN THE RABBIT TUBE WATER.

C

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DIMENSION R(8),RH04(50),RH08(50),
XSTORE(50),
XT(8,50),TFL0W(50),TP0SN(50),
XVEQUIV(50),VINTMD(50),VOL1(50),VOL3(50),VSTORE(50),
XYFLOW(50),YPOSN(50)
TYPE LOGICAL DEBUG
COMMON/1/DEBUG/2/TIME,TPOSN,YPOSN,PRABT/3/MPOSN/4/TFL0W,YFL0W,
XMFLOW,GPRIMARY,G1,G2,G3,GZERO/5/R/8/RNODE,RLNGTH,RH04,RHRVS4,
XMOVE,FACTOR,TRVRS4/9/T/10/JJ,K1,K2,KK1,KK2/14/BLANK3(102),RH08,
XBLANK4(100),D1,D2,D3,BLANK5(4),RBTRM,R3TRM2,TMPIN4,TMPIN8
X/15/IRABT,IRABT2,MRRVS/16/VOL3,VOLND3,STORE,DTAU,VOLND1,RBTNOD,
XRBTEND,RNDEND,RHRVS8,THRVS8
COMMON/18/STORE8(50)
1 FORMAT(10F12.4) REVR 18
2 FORMAT(10E12.4) REVR 19
3 FORMAT(10I12) REVR 20
4 FORMAT(/) REVR 21
5 FORMAT(34H COOLANT WATER EXPANSION TOO LARGE) REVR 22
6 FORMAT(E12.4,F12.4,21I2) REVR 23
7 FORMAT(2E12.4,I12,E12.4) REVR 24
8 FORMAT(1H1,17WSUBROUTINE REVRSE//) REVR 25
9 FORMAT(1X,I5) REVR 26
10 FORMAT(//96H RABBIT REVERSE VELOCITY EXCEEDS TUBE WATER REVERSE VEREVR 27
XLOCITY. INVALID INPUT. PROBLEM TERMINATED.) REVR 28
VOLEXS=0. REVR 29
L=1 REVR 30
M=0 REVR 31
IF(DEBUG) GO TO 100 REVR 32
PRINT 8 REVR 33
PRINT 4 REVR 34
PRINT 9, 9 REVR 35
PRINT 3, JJ,IRABT,K2,IRABT2,K1,MFL0W,MRRVS REVR 36
PRINT 2, VOLND3,D3,G3,DTAU,RNODE,VOLND1,RBTRM,RBTRM2,PRABT,RBTNOD,REVR 37
XRBTEND,RNDEND,TIME,GPRIMARY,G2,GZERO,RHRVS8,TRVRS8,G1,D1,RHRVS4, REVR 38
XTRVRS4,(VOL3(J),STORE(J),RH08(J),RH04(J),J=1,JJ),(R(I),I=1,8), REVR 39
X(TFL0W(1100),YFL0W(1100),I100=1,MFL0W),((T(I101,I102),I102=1,JJ), REVR 40
XI101=1,A) REVR 41
PRINT 4 REVR 42
100 CONTINUE REVR 43
DO 110 J=1,JJ REVR 44
110 STORE8(J)=STORE(J) REVR 45
VOLND1=3.1415927*(R(5)**2)*RNODE REVR 46
FACTOR=(R(5)**2-R(3)**2)/(R(5)**2) REVR 47
K501=K1-1 REVR 48
DO 250 J=1,K501 REVR 49
250 VOL1(J)=VOLND1 REVR 50
I15=K501+1 REVR 51
VOL1(I15)=RBTRM*VOLND1+(1,-RBTRM)*VOLND1*FACTOR REVR 52
I16=I15+1 REVR 53
DO 260 J=I16,K2 REVR 54
260 VOL1(J)=FACTOR*VOLND1 REVR 55
I17=K2+1 REVR 56
VOL1(I17)=RBTRM2*FACTOR*VOLND1+(1,-RBTRM2)*VOLND1 REVR 57
I18=I17+1 REVR 58
DO 270 J=I18,JJ REVR 59
270
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```

270 VOL1(J)=VOLND1
  IF(DEBUG) GO TO 280
  PRINT 4
  PRINT 9, 270
  PRINT 2, PRABT,RBTNOD,RBTRM,RBTEND,RNDEND,RBTRM2,VOLND1*FACTOR
  PRINT 3, IRABT,IRABT2,K1,K2
  PRINT 2, (VOL1(J),J=1,JJ)
280 CONTINUE
C
C
290 DO 300 J=1,JJ
300 VSTORE(J)=VOL1(J)
  IF(DEBUG) GO TO 310
  PRINT 4
  PRINT 9, 300
  PRINT 2, (VSTORE(J),J=1,JJ)
  PRINT 4
310 CONTINUE
  DO 320 J=1,JJ
  VINTMD(J)=VSTORE(J)*RH04(J)
  RH04(J)=DENSE(T(4,J))
320 VOL1(J)=VINTMD(J)/RH04(J)
  IF(DEBUG) GO TO 330
  PRINT 4
  PRINT 9, 320
  PRINT 2, (RH04(J),J=1,JJ)
  PRINT 4
  PRINT 2, (VOL1(J),J=1,JJ)
  PRINT 4
330 CONTINUE
  DO 340 J=1,JJ
340 STORE(J)=T(4,J)
  IF(DEBUG) GO TO 350
  PRINT 9, 340
  PRINT 1, (STORE(J),J=1,JJ)
  PRINT 4
350 CONTINUE
  VOLEXS=0.
  DO 390 J=2,JJ
  VOLEXS=VOLEXS+VOL1(J-1)-VSTORE(J-1)
  IF(VOLEXS-FACTOR*VOLND1)370,360,360
360 PRINT 5
  MRRVS=1
  GO TO 580
370 CONTINUE
  T(4,J)=(VOLEXS*RH04(J-1)*STORE(J-1)+(VSTORE(J)-VOLEXS)*RH04(J))
  X*STORE(J))/(VOLEXS*RH04(J-1)+(VSTORE(J)-VOLEXS)*RH04(J))
  IF(DEBUG) GO TO 380
  PRINT 9, 370
  PRINT 2, VOLEXS,T(4,J)
  PRINT 4
380 CONTINUE
390 CONTINUE
  RMOVE=0.
  CALL RABTGO
  VOLREP=(G1*3.1415927*(R(5)**2)*DTAU)/RHRVS4)
  X=RMOVE*3.1415927*R(5)**2
  IF(VOLREP)391,590,392
391 PRINT 10
  STOP

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392 CONTINUE          REVR 121
  DO 400 J=1,JJ      REVR 122
400 VEQUIV(J)=VSTORE(J)/VSTORE(JJ)    REVR 123
  VRPEQV=VCLREP/VSTORE(JJ)           REVR 124
  IF(DEBUG) GO TO 401             REVR 125
  PRINT 9, 400                  REVR 126
  PRINT 2, (VEQUIV(J),J=1,JJ),(VSTORE(J),J=1,JJ),VRPEQV,VOLREP,G1,  REVR 127
  XR(5),DTAU,RHRVS4,RMOVE          REVR 128
401 CONTINUE          REVR 129
  DO 410 J=1,JJ      REVR 130
410 VSTORE(J)=VEQUIV(J)           REVR 131
  VADD=0.                      REVR 132
  DO 420 J=1,JJ      REVR 133
  VADD=VADD+VEQUIV(J)           REVR 134
  K=J                          REVR 135
  IF(VADD-VRPEQV)420,420,440    REVR 136
420 CONTINUE          REVR 137
  DO 430 J=1,JJ      REVR 138
430 T(4,J)=TRVRS4            REVR 139
  GO TO 580                  REVR 140
440 CONTINUE          REVR 141
  VEXEQV=VADD-VRPEQV          REVR 142
  IF(DEBUG) GO TO 450         REVR 143
  PRINT 9, 440                  REVR 144
  PRINT 2, VRPEQV,VADD,VEXEQV   REVR 145
  PRINT 3, K                  REVR 146
450 CONTINUE          REVR 147
  DO 460 J=1,JJ      REVR 148
460 CALL WATER(T(4,J),D1,G1,MLDUMB,RHO4(J),CPDUMB)    REVR 149
  DO 470 J=1,JJ      REVR 150
470 STORE(J)=T(4,J)           REVR 151
  IF(DEBUG) GO TO 480         REVR 152
  PRINT 4                  REVR 153
  PRINT 9, 470                  REVR 154
  PRINT 2, (RHO4(J),J=1,JJ)    REVR 155
  PRINT 4                  REVR 156
  PRINT 1, (STORE(J),J=1,JJ)   REVR 157
  PRINT 4                  REVR 158
480 CONTINUE          REVR 159
  I20=K-1                  REVR 160
  KEXIT=K                  REVR 161
490 DO 500 L=1,I20          REVR 162
500 T(4,K)=(VEQUIV(K)-VEXEQV)*TRVRS4*RHRVS4+VEXEQV*STORE(1)*RHO4(1)/REVR 163
 X((VEQUIV(K)-VEXEQV)*RHRVS4*VEXEQV*RHO4(1))           REVR 164
  IF(K-JJ)510,580,580          REVR 165
510 I21=I20+2              REVR 166
  VLEFT=VEQUIV(1)-VEXEQV      REVR 167
  LINCRS=1                  REVR 168
  INCRS=0                  REVR 169
  DO 570 J=I21,JJ          REVR 170
  XNMRTR=0                  REVR 171
  INNER=0                  REVR 172
  DENMTR=0                  REVR 173
  M=J+1-KEXIT-LINCRS+INCRS   REVR 174
  IF(DEBUG) GO TO 519         REVR 175
  PRINT 9, 510                  REVR 176
  PRINT 3, J,INNER,M          REVR 177
  PRINT 2, XNMRTR,DENMTR,VEQUIV(J),VLEFT    REVR 178
519 CONTINUE          REVR 179

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```

520 IF(VLEFT-VEQUIV(J))530,560,560
530 XNMRTR=VLEFT+STORE(M)*RH04(M)+XNMRTR
DENMTR=VLEFT*RHO4(M)+DENMTR
VEQUIV(J)=VEQUIV(J)-VLEFT
MINUS=M+1
VLEFT=VSTORE(MINUS)
IF(DEBUG) GO TO 539
PRINT 9, 530
PRINT 3, MINUS
PRINT 2, XNMRTR,DENMTR,VEQUIV(J),VLEFT
539 CONTINUE
IF(VLEFT-VEQUIV(J))540,540,550
540 IMARK=M+1+INNER
XNMRTR=VLEFT+STORE(IMARK)*RH04(IMARK)+XNMRTR
DENMTR=VLEFT*RHO4(IMARK)+DENMTR
VEQUIV(J)=VEQUIV(J)-VLEFT
IMARK2=IMARK+1
VLEFT=VSTORE(IMARK2)
INCRES=INCRES+1
INNER=INNER+1
IF(DEBUG) GO TO 549
PRINT 9, 540
PRINT 3, IMARK,IMARK2,INCRES,INNER
PRINT 2, XNMRTR,DENMTR,VEQUIV(J),VLEFT
549 CONTINUE
IF(VLEFT-VEQUIV(J))540,540,550
550 IMARK=M+1+INNER
XNMRTR=XNMRTR+VEQUIV(J)*STORE(IMARK)*RH04(IMARK)
DENMTR=DENMTR+VEQUIV(J)*RHO4(IMARK)
T(4,J)=XNMRTR/DENMTR
VLEFT=VLEFT-VEQUIV(J)
IF(DEBUG) GO TO 559
PRINT 9, 550
PRINT 3, IMARK
PRINT 2, XNMRTR,DENMTR,T(4,J),VLEFT
559 CONTINUE
GO TO 570
560 T(4,J)=STORE(M)
VLEFT=VLEFT-VEQUIV(J)
LINCRS=LINCRS+1
IF(DEBUG) GO TO 569
PRINT 9, 560
PRINT 3, LINCRS
PRINT 2, T(4,J),VLEFT
569 CONTINUE
570 CONTINUE
580 CONTINUE
IF(DEBUG) GO TO 590
PRINT 4
PRINT 9, 580
PRINT 1, (T(4,J),J=1,JJ)
PRINT 3, JJ,IRABT,K2,IRABT2,K1,MFLOW,MRVRS
PRINT 2, VOLND3,D3,G3,DTAU,RNODE,VOLND1,RBTRM,RBTRM2,PRABT,RBTNOD,REVR 233
XRBTTEND,RNDEND,TIME,GPRIMARY,G2,GZEMO,RHRVS8,TRVRS8,G1,D1,RHRVS4, REVR 234
XTRVRS4,(VOL3(J),STCRE(J),RM08(J),RH04(J),J=1,JJ),(R(I),I=1,8), REVR 235
X(TFLOW(1100),YFLOW(1100),I100=1,MFLOW),((T(I101,I102),I102=1,JJ), REVR 236
X,I101=1,8) REVR 237
PRINT 4
590 RETURN
END REVR 239
REVR 240

```

SUBROUTINE PREVRE

```

C THIS SUBROUTINE IS USED TO DETERMINE THE FLOW-REVERSAL WATER
C TEMPERATURE ADJUSTMENT IN THE WATER CELL SURROUNDING THE RABBIT
C TUBE.
C
C DIMENSION R(8),RH04(50),RH08(50),
C XSTORE(50),
C XT(8,50),TFLW(50),TPOSN(50),
C XVEQUIV(50),VINTMD(50),VOL1(50),VOL3(50),VSTORE(50),
C XYFLOW(50),YPOSN(50)
C TYPE LOGICAL DEBUG
C COMMON/1/DEBUG/2/TIME,TPCSN,YPOSN,PRABT/3/MPOSN/4/TFLW,YFLOW,
C XMFLOW,GPRIMARY,G1,G2,G3,GZERO/5/R/8/RNODDE,RNGTH,RH04,RHRVS4,
C XMOVE,FACTOR,TRVRSS/9/T/10/J,J,K1,K2,KK1,KK2/14/BLANK3(102),RH08,
C XBLANK4(100),D1,D2,D3,BLANK5(4),RBTMH,RBTMR2,TMPIN4,TMPIN8
C X/15/IRART,IRABT2,RHRVS/16/VOL3,VOLND3,STORE,DTAU,VOLND1,RBTNOD,
C XRBTEND,RNDEND,RHRVS8,THRVS8
C COMMON/18/STORE8(50)
1 FORMAT(10F12.4)
2 FORMAT(10E12.4)
3 FORMAT(10I12)
4 FORMAT(/)
5 FORMAT(34H COOLANT WATER EXPANSION TOO LARGE)
6 FORMAT(E12.4,F12.4,2I12)
7 FORMAT(2E12.4,I12,E12.4)
8 FORMAT(1H1,17HSUBROUTINE REVRSE//)
9 FORMAT(1X,15)
VOLEXS=0.
L=1
M=0
DO 150 J=2,JJ
VOLEXS=VOLEXS+VOL3(J=L)-VOLND3
IF(VOLND3-VOLEXS)110,120,120
110 T(8,J)=STORE8(J=L)
VOLEXS=VOLEXS-VOLND3
M=M+1
L=L+1
GO TO 130
120 CONTINUE
T(8,J)=(VOLEXS*RH08(J-L)*STORE8(J-L)+(VOLND3-VOLEXS)*RH08(J-M)
X*STORE8(J-M))/(VOLEXS*RH08(J-L)+(VOLND3-VOLEXS)*RH08(J-M))
130 CONTINUE
IF(DEBUG) GO TO 140
PRINT 9, 130
PRINT 6, VOLEXS,T(8,J),M,L
140 CONTINUE
150 CONTINUE
DO 160 J=1,JJ
160 RH08(J)=DENSE(T(8,J))
IF(DEBUG) GO TO 170
PRINT 4
PRINT 9, 170
PRINT 1, (RH08(J),J=1,JJ)
PRINT 4
170 CONTINUE
C
C DO 180 J=1,JJ
180 STORE(J)=T(8,J)

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IF(DEBUG) GO TO 190          PREV  61
PRINT 9, 180                  PREV  62
PRINT 1, (STORE(J),J=1,JJ)    PREV  63
PRINT 4                        PREV  64
190 CONTINUE                   PREV  65
VOLREP=(G3*3.1415927*(R(8)**2*R(7)**2)*DTAU)/RHRVS8  PREV  66
ADVNC=VOLREP/VOLND3          PREV  67
I=ADVNC                      PREV  68
REMAIN=ADVNC-I                PREV  69
IF(DEBUG) GO TO 200          PREV  70
PRINT 4                        PREV  71
PRINT 9, 190                  PREV  72
PRINT 7, VOLREP,ADVNC,I,REMAIN  PREV  73
200 CONTINUE                   PREV  74
DO 210 J=1,I                  PREV  75
210 T(8,J)=TRVRS8            PREV  76
INTERM=I+1                    PREV  77
T(8,INTERM)=(REMAIN*TRVRS8*RHRVS8+(1.-REMAIN)*STORE(1)  PREV  78
X*RHO8(1))/(REMAIN*RHRVS8+(1.-REMAIN)*RHO8(1))        PREV  79
IJKLMN=I+2                    PREV  80
DO 220 J=IJKLMN,JJ           PREV  81
220 T(8,J)=(REMAIN*STORE(J-I+1)*RHO8(J-I-1)+(1.-REMAIN)*STORE(J-I)  PREV  82
X*RHO8(J-I))/(REMAIN*RHO8(J-I-1)+(1.-REMAIN)*RHO8(J-I))  PREV  83
C
DO 230 J=1,JJ                  PREV  84
230 RHO8(J)=DENSE(T(8,J))    PREV  85
C
IF(DEBUG) GO TO 240          PREV  86
PRINT 4                        PREV  87
PRINT 9, 230                  PREV  88
PRINT 1, (T(8,J),J=1,JJ)      PREV  89
PRINT 4                        PREV  90
PRINT 1, (RHO8(J),J=1,JJ)     PREV  91
PRINT 4                        PREV  92
PRINT 4                        PREV  93
PRINT 4                        PREV  94
240 CONTINUE                   PREV  95
C
RETURN                         PREV  96
END                            PREV  97

```

SUBROUTINE POSITN	POSI
C	POSI
THIS SUBROUTINE IS USED TO DETERMINE THE TIME-DEPENDENT RABBIT	1
VERTICAL POSITION.	2
C	POSI
DIMENSION X(50),	3
XY(50)	4
COMMON/2/TIME,X,Y,Z/3/M	5
1 FORMAT(23H0INDEPENDENT VARIABLE (,E12.5,1X,	6
X37H) OUT OF RANGE....PROBLEM TERMINATED/)	7
N=2	POSI
IF(X(1)-TIME*3600.)110,100,160	8
100 Z=Y(1)	9
GO TO 170	10
110 IF(TIME*3600.-X(M))120,120,160	11
120 IF(TIME*3600.-X(N))130,140,150	12
130 Z=((TIME*3600.-X(N-1))/(X(N)-X(N-1)))*(Y(N)-Y(N-1))+Y(N-1)	13
GO TO 170	14
140 Z=Y(N)	15
GO TO 170	16
150 N=N+1	17
GO TO 110	18
160 TPRINT=TIME*3600.	19
PRINT 1, TPRINT	20
TIME=-20.	21
GO TO 180	22
170 CONTINUE	23
180 CONTINUE	24
Z=Z/12.	25
RETURN	26
END	27
	28
	29
	30
	31

SUBROUTINE RABTGO

THIS SUBROUTINE IS USED TO DETERMINE THE RABBIT POSITION  
ADJUSTMENT DURING THE RABBIT EJECTION PHASE.

```

C      DIMENSION RH04(50),
C      XT(8,50),TKEEP(3,50),TP0SN(50),TRBT1(3),TRBT2(3),TSTORE(50),
C      YPOSN(50)
C      TYPE LOGICAL DEBUG
C      COMMON/1/DEBUG/2/TIME,TP0SN,YPOSN,PRABT/3/MPOSN/8/RNODE,RLNGTH,
C      XRHO4,RHRS4,RMOVE,FACTOR,THVRS4/9/T/10/JJ,K1,K2,KK1,KK2
C
C      1 FORMAT(1H1,17HSUBROUTINE RABTGO//)
C      2 FORMAT(1X,I5)
C      3 FORMAT(1X,E11.5,9E12.5)
C      4 FORMAT(10I12)
C      8 FORMAT(/)

C      70 CONTINUE
C      DO 100 J=1,JJ
C      100 TSTORE(J)=T(4,J)
C      IF(DEBUG) GO TO 9000 $ PRINT 1 $ PRINT 2, 100
C      PRINT 3, (TSTORE(J),J=1,JJ) $ PRINT 8
C      9000 CONTINUE
C      DO 120 J=K1,K2
C      DO 110 I=1,3
C      110 TKEEP(I,J)=T(I,J)
C      120 CONTINUE
C      IF(DEBUG) GO TO 9010 $ PRINT 2, 110 $ PRINT 4, JJ,K1,K2
C      PRINT 3, ((TKEEP(I,J),I=1,3),J=K1,K2) $ PRINT 8
C      9010 CONTINUE
C      STORE1=PRABT
C      STORE2=PRABT/RNODE
C      ISTOR3=STORE2
C      STORE4=STORE2-ISTOR3
C      STORE5=(PRABT+RLNGTH)/RNODE
C      ISTOR6=STORE5
C      STORE7=STORE5-ISTOR6
C      ISTOR8=K1
C      ISTOR9=K2
C      IF(DEBUG) GO TO 9020 $ PRINT 2, 120
C      PRINT 4, ISTOR3,ISTOR6,ISTOR8,ISTOR9
C      PRINT 3, STORE1,STORE2,STORE4,STORE5,STORE7 $ PRINT 8
C      9020 CONTINUE
C      IF(ISTOR8-JJ)130,130,920
C      130 IF(STORE4,.5)160,160,140
C      140 IF(ISTOR8*2-JJ)145,145,141
C      141 IF(ISTOR8*1-JJ)142,142,144
C      142 DO 143 I=1,3
C      143 TRBT1(I)=2.*TKEEP(I,ISTOR8)-TKEEP(I,ISTOR8+1)
C      GO TO 151
C      144 DO 146 I=1,3
C      146 TRBT1(I)=TKEEP(I,ISTOR8)
C      GO TO 151
C      145 DO 150 I=1,3
C      150 TRBT1(I)=TKEEP(I,ISTOR8+2)+3.*TKEEP(I,ISTOR8+1)+3.*TKEEP(I,ISTOR8)
C      151 CONTINUE
C      IF(DEBUG) GO TO 9030 $ PRINT 2, 150 $ PRINT 3, (TRBT1(I),I=1,3)
C      PRINT 8
C      9030 CONTINUE

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```

160 CONTINUE RABT 61
  IF(ISTOR9-JJ)170,170,920 RABT 62
170 IF(STORE7-.5)180,180,200 RABT 63
180 DO 190 I=1,3 RABT 64
190 TRBT2(I)=TKEEP(I,ISTOR9-2)+3.*TKEEP(I,ISTOR9-1)+3.*TKEEP(I,ISTOR9) RABT 65
  IF(DEBUG) GO TO 9040 $ PRINT 2, 190 $ PRINT 3, (TRBT2(I),I=1,3) RABT 66
    PRINT 8 RABT 67
9040 CONTINUE RABT 68
200 CONTINUE RABT 69
C CALL POSITN RABT 70
C
  RMOVE=PRABT+STORE1 RABT 71
  IF(DEBUG) GO TO 9050 $ PRINT 2, 200 $ PRINT 3, RMOVE $ PRINT 8 RABT 72
9050 CONTINUE RABT 73
  IF(RMOVE)1050,1050,210 RABT 74
210 RBTNOD=PRABT/RNODE RABT 75
  IRABT=RBTNOD RABT 76
  RBTRM=RBTNOD-IRABT RABT 77
  IF(DEBUG) GO TO 9060 $ PRINT 2, 210 $ PRINT 4, IRABT RABT 78
  PRINT 3, RBTNOD,RBTRM $ PRINT 8 RABT 79
9060 CONTINUE RABT 80
  IF(RBTRM-.5)220,220,230 RABT 81
220 K1=IRABT+1 RABT 82
  IF(DEBUG) GO TO 9070 $ PRINT 2, 220 $ PRINT 4, K1 $ PRINT 8 RABT 83
9070 CONTINUE RABT 84
  GO TO 240 RABT 85
230 K1=IRABT+2 RABT 86
  IF(DEBUG) GO TO 9080 $ PRINT 2, 230 $ PRINT 4, K1 $ PRINT 8 RABT 87
9080 CONTINUE RABT 88
240 CONTINUE RABT 89
  RBTEND=PRABT+RLNGTH RABT 90
  RNDEND=RBTEND/RNODE RABT 91
  IRABT2=RNDEND RABT 92
  RBTRM2=RNDEND-IRABT2 RABT 93
  IF(DEBUG) GO TO 9090 $ PRINT 2, 240 $ PRINT 4, IRABT2 RABT 94
  PRINT 3, RBTEND,RNDEND,RETHM2 $ PRINT 8 RABT 95
9090 CONTINUE RABT 96
  IF(RBTRM2-.5)250,250,260 RABT 97
250 K2=IRABT2 RABT 98
  IF(DEBUG) GO TO 9100 $ PRINT 2, 250 $ PRINT 4, K2 $ PRINT 8 RABT 99
9100 CONTINUE RABT 100
  GO TO 270 RABT 101
260 K2=IRABT2+1 RABT 102
  IF(DEBUG) GO TO 9110 $ PRINT 2, 260 $ PRINT 4, K2 $ PRINT 8 RABT 103
9110 CONTINUE RABT 104
270 CONTINUE RABT 105
  KK1=K1+1 RABT 106
  KKK2=K2+1 RABT 107
  EMOVE=RMOVE/RNODE RABT 108
  IMOVE=EMOVE RABT 109
  EREMAN=EMOVE-IMOVE RABT 110
  IF(DEBUG) GO TO 9120 $ PRINT 2, 270 $ PRINT 4, KK1,KKK2,IMOVE RABT 111
  PRINT 3, EMOVE,EREMAN $ PRINT 8 RABT 112
9120 CONTINUE RABT 113
C
  IF(K1-JJ)280,280,920 RABT 114
280 CONTINUE RABT 115
  IF(STORE4-.5)500,500,290 RABT 116
290 IF(EREMAN-(1,-STORE4))300,300,380 RABT 117
                                         RABT 118
                                         RABT 119
                                         RABT 120

```

```

300 DO 310 I=1,3          RABT 121
310 T(I,K1)=EREMAN*TRBT1(I)+(1.-EREMAN)*TKEEP(I,ISTOR8) RABT 122
  IF(DEBUG) GO TO 9130 $ PRINT 2, 310 $ PRINT 3, (T(I,K1),I=1,3) RABT 123
  PRINT 8 RABT 124
9130 CONTINUE RABT 125
  IF(K1+1-JJ)320,320,920 RABT 126
320 IEND1=K1+1 RABT 127
  IF(DEBUG) GO TO 9140 $ PRINT 2, 320 $ PRINT 4, IEND1 $ PRINT 8 RABT 128
9140 CONTINUE RABT 129
  IF(K2+1-JJ)330,340,340 RABT 130
330 IEND2=K2+1 RABT 131
  IF(DEBUG) GO TO 9150 $ PRINT 2, 330 $ PRINT 4, IEND2 $ PRINT 8 RABT 132
9150 CONTINUE RABT 133
  GO TO 350 RABT 134
340 IEND2=JJ RABT 135
  IF(DEBUG) GO TO 9160 $ PRINT 2, 340 $ PRINT 4, IEND2 $ PRINT 8 RABT 136
9160 CONTINUE RABT 137
350 DO 370 J=IEND1,IEND2 RABT 138
  IRACK=J-IMOVE+1 RABT 139
  DO 360 I=1,3 RABT 140
360 T(I,J)=EREMAN*TKEEP(I,IBACK)+(1.-EREMAN)*TKEEP(I,IBACK+1) RABT 141
370 CONTINUE RABT 142
  IF(DEBUG) GO TO 9170 $ PRINT 2, 360 RABT 143
  PRINT 3, ((T(I,J),I=1,3),J=IEND1,IEND2) $ PRINT 8 RABT 144
9170 CONTINUE RABT 145
  GO TO 700 RABT 146
C
380 CONTINUE RABT 147
  IF(RBTRM-.5)410,410,390 RABT 148
390 DO 400 I=1,3 RABT 149
400 T(I,K1)=EREMAN*TKEEP(I,ISTUR8)+(1.-EREMAN)*TKEEP(I,ISTOR8+1) RABT 150
  IF(DEBUG) GO TO 9180 $ PRINT 2, 400 $ PRINT 3, (T(I,K1),I=1,3) RABT 151
  PRINT 8 RABT 152
9180 CONTINUE RABT 153
  GO TO 430 RABT 154
410 DO 420 I=1,3 RABT 155
420 T(I,K1)=((1.-STORE4)*TRBT1(I)+(STORE4-RBTRM)*TKEEP(I,ISTOR8)) RABT 156
  X/(1.-RBTRM) RABT 157
  IF(DEBUG) GO TO 9190 $ PRINT 2, 420 $ PRINT 3, (T(I,K1),I=1,3) RABT 158
  PRINT 8 RABT 159
9190 CONTINUE RABT 160
430 CONTINUE RABT 161
  IF(K1+1-JJ)440,440,920 RABT 162
440 IEND1=K1+1 RABT 163
  IF(DEBUG) GO TO 9200 $ PRINT 2, 440 $ PRINT 4, IEND1 $ PRINT 8 RABT 164
9200 CONTINUE RABT 165
  IF(K2+1-JJ)450,450,460 RABT 166
450 IEND2=K2+1 RABT 167
  IF(DEBUG) GO TO 9210 $ PRINT 2, 450 $ PRINT 4, IEND2 $ PRINT 8 RABT 168
9210 CONTINUE RABT 169
  GO TO 470 RABT 170
460 IEND2=JJ RABT 171
  IF(DEBUG) GO TO 9220 $ PRINT 2, 460 $ PRINT 4, IEND2 $ PRINT 8 RABT 172
9220 CONTINUE RABT 173
470 DO 490 J=IEND1,IEND2 RABT 174
  IRACK=J-IMOVE+1 RABT 175
  DO 480 I=1,3 RABT 176
480 T(I,J)=EREMAN*TKEEP(I,IBACK)+(1.-EREMAN)*TKEEP(I,IBACK+1) RABT 177
490 CONTINUE RABT 178
  IF(DEBUG) GO TO 9230 $ PRINT 2, 480 RABT 179

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```

      PRINT 3, ((T(I,J),I=1,3),J=IEND1,IEND2) $ PRINT 8          RABT 181
9230 CONTINUE
      GO TO 710
C
 500 CONTINUE
  IF(EREMAN-(.5-STORE4))510,510,590
510 DO 520 I=1,3
520 T(I,K1)=T(I,ISTOR8)
  IF(DEBUG) GO TO 9240 $ PRINT 2, 520 $ PRINT 3, (T(I,K1),I=1,3)
  PRINT 8
9240 CONTINUE
  IF(K1+1-JJ)530,530,920
530 IEND1=K1+1
  IF(DEBUG) GO TO 9250 $ PRINT 2, 530 $ PRINT 4, IEND1 $ PRINT 8
9250 CONTINUE
  IF(K2-1-JJ)540,550,550
540 IEND2=K2+1
  IF(DEBUG) GO TO 9260 $ PRINT 2, 540 $ PRINT 4, IEND2 $ PRINT 8
9260 CONTINUE
  GO TO 560
550 IEND2=JJ
  IF(DEBUG) GO TO 9270 $ PRINT 2, 550 $ PRINT 4, IEND2 $ PRINT 8
9270 CONTINUE
560 DO 580 J=IEND1,IEND2
  IBACK=J-IMOVE-1
  DO 570 I=1,3
570 T(I,J)=EREMAN*TKEEP(I,IBACK)+(1,-EREMAN)*TKEEP(I,IBACK+1)
580 CONTINUE
  IF(DEBUG) GO TO 9280 $ PRINT 2, 570
  PRINT 3, ((T(I,J),I=1,3),J=IEND1,IEND2) $ PRINT 8
9280 CONTINUE
  GO TO 710
C
 590 CONTINUE
  IF(EREMAN-(1.-STORE4))620,620,600
600 DO 610 I=1,3
610 T(I,K1)=((1.-STORE4)*TKEEP(I,ISTOR8)+(1.-EREMAN)*TKEEP(I,ISTOR8+1))
X)/(2.-STORE4-EREMAN)
  IF(DEBUG) GO TO 9290 $ PRINT 2, 610 $ PRINT 3, (T(I,K1),I=1,3)
  PRINT 8
9290 CONTINUE
  GO TO 640
620 DO 630 I=1,3
630 T(I,K1)=EREMAN*TKEEP(I,ISTOR8)+(1.-EREMAN)*TKEEP(I,ISTOR8+1)
  IF(DEBUG) GO TO 9300 $ PRINT 2, 630 $ PRINT 3, (T(I,K1),I=1,3)
  PRINT 8
9300 CONTINUE
640 CONTINUE
  IF(K1+1-JJ)650,650,920
650 IEND1=K1+1
  IF(DEBUG) GO TO 9310 $ PRINT 2, 650 $ PRINT 4, IEND1 $ PRINT 8
9310 CONTINUE
  IF(K2-1-JJ)660,670,670
660 IEND2=K2+1
  IF(DEBUG) GO TO 9320 $ PRINT 2, 660 $ PRINT 4, IEND2 $ PRINT 8
9320 CONTINUE
  GO TO 680
670 IEND2=JJ
  IF(DEBUG) GO TO 9330 $ PRINT 2, 670 $ PRINT 4, IEND2 $ PRINT 8
9330 CONTINUE

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680 DO 700 J=IEND1,IEND2          RABT 241
  IBACK=J-IMOVE-1                 RABT 242
  DO 690 I=1,3                     RABT 243
690 T(I,J)=EREMAN*TKEEP(I,IBACK)+(1,-EREMAN)*TKEEP(I,IBACK+1) RABT 244
700 CONTINUE                       RABT 245
  IF(DEBUG) GO TO 9340 $ PRINT 2, 690
  PRINT 3, ((T(I,J),I=1,3),J=IEND1,IEND2) $ PRINT 8           RABT 246
9340 CONTINUE                      RABT 247
C
710 IF(K2-JJ)720,720,910          RABT 248
720 IF(STORE7-.5)730,820,820      RABT 249
730 IF(STORE7+EREMAN-.5)740,740,760 RABT 250
740 DO 750 I=1,3                 RABT 251
750 T(I,K2)=EREMAN*TKEEP(I,ISTOR9-1)+(1,-EREMAN)*TKEEP(I,ISTOR9) RABT 252
  IF(DEBUG) GO TO 9350 $ PRINT 2, 750 $ PRINT 3, (T(I,K2),I=1,3) RABT 253
  PRINT 8                         RABT 254
9350 CONTINUE                      RABT 255
  GO TO 910                        RABT 256
C
760 CONTINUE                        RABT 257
  IF(STORE7+EREMAN-1.)790,790,770 RABT 258
770 DO 780 I=1,3                 RABT 259
780 T(I,K2)=EREMAN*TKEEP(I,ISTOR9)+(1,-EREMAN)*TRBT2(I)        RABT 260
  IF(DEBUG) GO TO 9360 $ PRINT 2, 780 $ PRINT 3, (T(I,K2),I=1,3) RABT 261
  PRINT 8                         RABT 262
9360 CONTINUE                      RABT 263
  GO TO 810                        RABT 264
790 DO 800 I=1,3                 RABT 265
800 T(I,K2)=(EREMAN*TKEEP(I,ISTOR9)+STORE7*TRBT2(I))/(EREMAN+STORE7) RABT 266
  IF(DEBUG) GO TO 9370 $ PRINT 2, 800 $ PRINT 3, (T(I,K2),I=1,3) RABT 267
  PRINT 8                         RABT 268
9370 CONTINUE                      RABT 269
810 CONTINUE                        RABT 270
  GO TO 910                        RABT 271
C
820 IF(STORE7+EREMAN-1.)830,830,850 RABT 272
830 DO 840 I=1,3                 RABT 273
840 T(I,K2)=(EREMAN*TKEEP(I,ISTOR9-1)+STORE7*TKEEP(I,ISTOR9))/(EREMAN
  *STORE7)
  IF(DEBUG) GO TO 9380 $ PRINT 2, 840 $ PRINT 3, (T(I,K2),I=1,3) RABT 274
  PRINT 8                         RABT 275
9380 CONTINUE                      RABT 276
  GO TO 910                        RABT 277
C
850 CONTINUE                        RABT 278
  IF(RBTRM2-.5)880,880,860       RABT 279
860 DO 870 I=1,3                 RABT 280
870 T(I,K2)=TKEEP(I,ISTOR9)        RABT 281
  IF(DEBUG) GO TO 9390 $ PRINT 2, 870 $ PRINT 3, (T(I,K2),I=1,3) RABT 282
  PRINT 8                         RABT 283
9390 CONTINUE                      RABT 284
  GO TO 900                        RABT 285
880 DO 890 I=1,3                 RABT 286
890 T(I,K2)=EREMAN*TKEEP(I,ISTOR9-1)+(1,-EREMAN)*TKEEP(I,ISTOR9) RABT 287
  IF(DEBUG) GO TO 9400 $ PRINT 2, 890 $ PRINT 3, (T(I,K2),I=1,3) RABT 288
  PRINT 8                         RABT 289
9400 CONTINUE                      RABT 290
900 CONTINUE                        RABT 291
C
910 CONTINUE                      RABT 292
                                         RABT 293
                                         RABT 294
                                         RABT 295
                                         RABT 296
                                         RABT 297
                                         RABT 298
                                         RABT 299
                                         RABT 300

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```

920 CONTINUE
  CHECK=REMOVE/RNODE
  ICHECK=CHECK
  EXCESS=CHECK-ICHECK
  IF(DEBUG) GO TO 9410 $ PRINT 2, 920 $ PRINT 4, ICHECK
  PRINT 3, CHECK,EXCESS $ PRINT 8
9410 CONTINUE
  IF(ICHECK)950,950,930
930 DO 940 I=1,ICHECK
  T(4,I)=TRVRS4
  IF(DEBUG) GO TO 9420 $ PRINT 2, 930 $ PRINT 3, T(4,I) $ PRINT 8
9420 CONTINUE
  IF(I-JJ)940,1050,1050
940 CONTINUE
950 ICK2=ICHECK+1
  T(4,ICK2)=(EXCESS*TRVRS4*RHHVS4+(1.-EXCESS)*TSTORE(1)*RH04(1))
  X*(EXCESS*RHRVS4+(1.-EXCESS)*RH04(1))
  ICK3=ICK2+1
  IF(DEBUG) GO TO 9430 $ PRINT 2, 950 $ PRINT 4, ICK2,ICK3
  PRINT 3, T(4,ICK2) $ PRINT 8
9430 CONTINUE
  DO 960 I=ICK3,IRABT
  M1=I-ICHECK-1
  MM1=I-ICHECK
  T(4,I)=(EXCESS*TSTORE(M1)*RH04(M1)+(1.-EXCESS)*TSTORE(MM1)*
  XRHO4(MM1))/(EXCESS*RHO4(M1)+(1.-EXCESS)*RHO4(MM1))
  IF(DEBUG) GO TO 9440 $ PRINT 2, 950 $ PRINT 3, T(4,I) $ PRINT 8
9440 CONTINUE
  IF(I-JJ)960,1050,1050
C
960 CONTINUE
  KADVNC=IRABT+1
  M2=KADVNC-ICHECK-1
  M3=KADVNC-ICHECK
  IF(DEBUG) GO TO 9450 $ PRINT 2, 960 $ PRINT 4, KADVNC,M2,M3
  PRINT 8
9450 CONTINUE
  IF(RBTRM-EXCESS)970,970,980
970 T(4,KADVNC)=(RBTRM*TSTORE( M2) *RH04(M2)
  X*(EXCESS-RBTRM)*FACTOR*TSTORE( M2) *RH04(M2)
  X*(1.-EXCESS)*FACTOR*TSTORE( M3) *RH04(M3))/
  X(RBTRM*RHO4(M2) +(EXCESS-RBTRM)*FACTOR*RHO4(M2)
  X +(1.-EXCESS)*FACTOR*RHO4(M3))
  IF(DEBUG) GO TO 9460 $ PRINT 2, 970 $ PRINT 3, T(4,KADVNC)
  PRINT 8
9460 CONTINUE
  GO TO 990
980 T(4,KADVNC)=(EXCESS*TSTORE(M2)*RH04(M2)+(RBTRM-EXCESS)*
  XTSTORE(M3)*RH04(M3)+FACTOR*(1.-RBTRM)*TSTORE(M3)*RH04(M3))
  X/(EXCESS*RHO4(M2)+(RBTRM-EXCESS)*RH04(M3)+FACTOR*(1.-RBTRM)
  X*RHO4(M3))
990 LADVNC=KADVNC+1
  IF(DEBUG) GO TO 9470 $ PRINT 2, 980 $ PRINT 4, LADVNC
  PRINT 3, T(4,KADVNC) $ PRINT 8
9470 CONTINUE
  DO 1000 I=LADVNC,IRABT2
  M4=I-ICHECK-1
  M5=I-ICHECK
  T(4,I)=(EXCESS*TSTORE( "4) *RH04(M4) +
  X*(1.-EXCESS)*TSTORE( M5) *RH04(M5))/

```

```

X(EXCESS*RHO4(M4)          +(1.-EXCESS)*RHO4(M5))      RABT 361
IF(DEBUG) GO TO 9480 $ PRINT 2, 990 $ PRINT 3, T(4,I) $ PRINT 8
9480 CONTINUE
IF(I-JJ)1000,1050,1050
1000 CONTINUE
KADVN2=IRABT2+1           RABT 362
M6=KADVN2-ICHECK-1        RABT 363
M7=KADVN2-ICHECK          RABT 364
IF(DEBUG) GO TO 9490 $ PRINT 2, 1000 $ PRINT 4, KADVN2,M6,M7
PRINT 8                    RABT 365
9490 CONTINUE
IF(RBTRM2-EXCESS)1020,1020,1010
1010 T(4,KADVN2)=(EXCESS*TSTORE( M6)          *RHO4(M6)      RABT 366
X*FACTOR*(RBTRM2-EXCESS)*TSTORE( M7)          *RHO4(M7)*    RABT 367
XFACTOR*(1.-RBTRM2)*TSTORE( M7)              *RHO4(M7))/    RABT 368
X(EXCESS*RHO4(M6)          )*FACTOR+(RBTRM2-EXCESS)*RHO4(M7) RABT 369
X*FACTOR*(1.-RBTRM2)*RHO4(M7)                RABT 370
IF(DEBUG) GO TO 9500 $ PRINT 2, 1010 $ PRINT 3, T(4,KADVN2) RABT 371
PRINT 8                    RABT 372
9500 CONTINUE
GO TO 1030
1020 T(4,KADVN2)=(RBTRM2*FACTOR*TSTORE(M6)*RHO4(M6)+(EXCESS-RBTRM2)
X*TSTORE(M6)*RHO4(M6)*(1.-EXCESS)*TSTORE(M7)*RHO4(M7)      RABT 373
X/(RBTRM2*FACTOR*RHO4(M6)*(EXCESS-RBTRM2)*RHO4(M6)*(1.-EXCESS)
X*RHO4(M7))          RABT 374
1030 KADVN3=KADVN2+1        RABT 375
IF(DEBUG) GO TO 9510 $ PRINT 2, 1020 $ PRINT 4, KADVN3
PRINT 3, T(4,KADVN2) $ PRINT 8
9510 CONTINUE
DO 1040 I=KADVN3,JJ
M8=I-ICHECK-1             RABT 376
M9=I-ICHECK               RABT 377
T(4,I)=(EXCESS*TSTORE( M8)          *RHO4(M8)+    RABT 378
X(1.-EXCESS)*TSTORE( M9)          *RHO4(M9)      RABT 379
X*RHO4(M8)                +(1.-EXCESS)*RHO4(M9))    RABT 380
1040 CONTINUE
IF(DEBUG) GO TO 9520 $ PRINT 2, 1030
PRINT 3, (T(4,I),I=KADVN3,JJ) $ PRINT 8
9520 CONTINUE
1050 RETURN
END

```

SUBROUTINE QHEAT

C THIS SUBROUTINE IS USED TO DETERMINE THE TIME-DEPENDENT AND  
C POSITION-DEPENDENT HEATING RATE OF A HYDRAULIC RABBIT ASSEMBLY.  
C

```

DIMENSION HEAT(50),
QCAL(50),QH20(50),
XX(50),
XY(50)
COMMON/2/TIME,BLANK1(101)/10/JJ,IBLANK1(4)/11/HEAT,X,Y,QH20,QAL,
XQMAXW,QMAXM/12/M
1 FORMAT(23H0INDEPENDENT VARIABLE (,E12.5,1X,
X37H) OUT OF RANGE....PROBLEM TERMINATED/)
N=2
IF(X(1)-TIME*3600.)110,100,160
100 QVSTIM=Y(1)
GO TO 170
110 IF(TIME*3600.-X(M))120,120,160
120 IF(TIME*3600.-X(N))130,140,150
130 QVSTIM=((TIME*3600.-X(N-1))/(X(N)-X(N-1)))*(Y(N)-Y(N-1))+Y(N-1)
GO TO 170
140 QVSTIM=Y(N)
GO TO 170
150 N=N+1
GO TO 110
160 TPRINT=TIME*3600.
PRINT 1,TPRINT
TIME=-20.
GO TO 190
170 CONTINUE
DO 180 J=1,JJ
QH20(J)=QMAXW*HEAT(J)*QVSTIM
180 QAL(J)=QMAXM*HEAT(J)*QVSTIM
190 CONTINUE
RETURN
END

```

SUBROUTINE WATER(T,D,G,HL,HMO,CP)

C THIS SUBROUTINE IS USED TO DETERMINE WATER AND HEAT TRANSFER  
C PROPERTIES AS A FUNCTION OF TEMPERATURE, FLOW RATE, AND GEOMETRY.

```

RH0=62.19615+1.269555*(T/100.)*1.952005*((T/100.)**2)
X*.5637521*((T/100.)*3)-.08217391*((T/100.)**4)
VISC=7.694890-.1387822*T*.1209692*((T/10.)**2)
X*.086437*((T/100.)*3)+.8175711*((T/100.)**4)
COND=.33293*,00031481481*T
CP=.9970146*,1777121*((T/1000.)*2,089844*((T/1000.)**2)
X*12,29523*((T/1000.)*3)+8.33239*((T/1000.)**4)
HL=(.023*COND/D)*((D*ABSF(G)/VISC)**.8)*((CP*VISC/COND)**.4)
RETURN
END

```

FUNCTION DENSE(T)

C THIS FUNCTION IS USED TO DETERMINE THE TEMPERATURE-DEPENDENT  
C DENSITY OF WATER.

```

DENSE=62.19615+1.269555*(T/100.)*1.952005*((T/100.)**2)
X*.5637521*((T/100.)*3)-.08217391*((T/100.)**4)
RETURN
END

```

QHEA	1
QHEA	2
QHEA	3
QHEA	4
QHEA	5
QHEA	6
QHEA	7
QHEA	8
QHEA	9
QHEA	10
QHEA	11
QHEA	12
QHEA	13
QHEA	14
QHEA	15
QHEA	16
QHEA	17
QHEA	18
QHEA	19
QHEA	20
QHEA	21
QHEA	22
QHEA	23
QHEA	24
QHEA	25
QHEA	26
QHEA	27
QHEA	28
QHEA	29
QHEA	30
QHEA	31
QHEA	32
QHEA	33
QHEA	34
QHEA	35
QHEA	36

WATE	1
WATE	2
WATE	3
WATE	4
WATE	5
WATE	6
WATE	7
WATE	8
WATE	9
WATE	10
WATE	11
WATE	12
WATE	13
WATE	14
WATE	15

DENS	1
DENS	2
DENS	3
DENS	4
DENS	5
DENS	6
DENS	7
DENS	8
DENS	9

```

C SUBROUTINE GAUSS1(ARRAY,N,U)
C THIS SUBROUTINE IS USED TO SOLVE A SET OF SIMULTANEOUS EQUATIONS
C USING THE METHOD OF GAUSS.
C
DIMENSION ARRAY(8,8),A(8),B(8),C(8),D(8),ALPHA(8),S(8)
NN=N-1
B(1)=ARRAY(1,1)
C(1)=-ARRAY(1,2)
DO 100 I=2,NN
II=I-1
III=I+1
A(I)=-ARRAY(I,II)
B(I)=ARRAY(I,I)
100 C(I)=-ARRAY(I,III)
A(N)=-ARRAY(N,NN)
B(N)=ARRAY(N,N)
ALPHA(1)=B(1)
DO 110 I=2,N
II=I-1
110 ALPHA(I)=B(I)-A(I)*C(II)/ALPHA(II)
S(1)=D(1)
DO 120 I=2,N
II=I-1
120 S(I)=D(I)+A(I)*S(II)/ALPHA(II)
D(N)=S(N)/ALPHA(N)
DO 130 I=1,NN
II=NN-I+1
III=II+1
130 D(II)=(S(II)+C(II)*D(III))/ALPHA(II)
RETURN
END
GAUS 1
GAUS 2
GAUS 3
GAUS 4
GAUS 5
GAUS 6
GAUS 7
GAUS 8
GAUS 9
GAUS 10
GAUS 11
GAUS 12
GAUS 13
GAUS 14
GAUS 15
GAUS 16
GAUS 17
GAUS 18
GAUS 19
GAUS 20
GAUS 21
GAUS 22
GAUS 23
GAUS 24
GAUS 25
GAUS 26
GAUS 27
GAUS 28
GAUS 29
GAUS 30
GAUS 31
GAUS 32

```

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